FACT SHEET

(Pursuant to Nevada Administrative Code (NAC) 445A.401)

Permittee Name: **Quartz Lake Mining, Inc.**

Project Name: **Red Rock Mill Project**

Permit Number: **NEV2022119**

Review Type/Year/Revision: **New 2023, Fact Sheet Revision 00**

A. Location and General Description

Location: The Project site is located in the Soda Springs Valley approximately one-half mile northeast of the town of Mina, in Mineral County, Nevada. The project is located in Section 5, Township 6 North, Range 35 East, Mount Diablo Baseline and Meridian. The Red Rock Mill project site is comprised of 11 unpatented mill site claims located entirely on public lands administered by the Bureau of Land Management (BLM) Stillwater Field Office. Quartz Lake Mining, Inc. (QLM) is the Permittee, and operator of the property.

The access route to the Project is from US Highway 95 approximately one-half mile north of the northern outskirts of Mina to Simon Lead Road. Then easterly on Simon Lead Road 0.4 miles to the Project entrance gate. The approximate center of the Project area is 4,251,060 North, 403,110 East, UTM meters NAD83 projection.

General Description: The Permittee is proposing to put the existing 200-ton per day mill back into production on the existing mill site. The Project includes a Crushing Plant, a Mill with gravity and flotation beneficiation circuits, solution conveyance pipelines, a Tailing Storage Facility (TSF), an Ore Stockpile Facility (OSF), an office, an assay lab, and a maintenance shop. The current facility was last operated for a brief period of time in the 1980s. When the facility was put into temporary closure in the 1980s the mill building, and equipment were thoroughly cleaned and left in an operational state. The facility requires minor rehabilitation of the existing concrete containment and equipment. Line power and municipal water supply hookups remained operational. The mill is designed to process gold and other metallic ores to produce both gravity and flotation concentrates. New tailings ponds will be constructed prior to facility startup.

B. Synopsis

Geology: The geology of the Project site and that area up to and beyond a 1-mile radius is identified as desert wash and alluvium. These alluvial deposits include surficial deposits of the diversified lithology, such as playa hard clay, with associated local evaporite deposits of salt, sodium carbonate, and borax; gravel and boulder veneers carried by flash floods from the mountains to the borders of the playas. The area includes “beach deposits” of earlier lakes, including those contemporaneous with the last high stage of Pleistocene Lake Lahontan. This description is in keeping with well driller log data from the area that exceeds the 100-foot depth minimum.

History: Historically, the Red Rock Mill has been a custom milling facility that has operated under various configurations to meet the specific requirements of prior operators, possibly as far back as the late 1950s. Ore from various local or regional sources was hauled to the mill, custom milled, and processed for the production of gold and silver. Anecdotal information indicates that in addition to silver and gold production, barite, tungsten, and decorative rock were also processed in small quantities in the past. Originally a cyanide facility, it has since been converted and is now a gravity and flotation circuit only. Several site assessments conducted in the summer of 2007 indicate that the current mill facility was installed between 1981 and 1982. The mill operated on a sporadic basis between 1981and 1986, at which time a Notice-of-Intent with the BLM was submitted. Additional processing equipment appears to have been installed since that time but not operated. The BLM approved a Plan of Operation and issued a Finding of No Significant Impact and Decision Record on 2 February 2010 to operate the facility with gravity and flotation circuits only.

Infrastructure Materials Corp. sold the property to QLM on 10 November 2021. QLM immediately began permitting the facility for processing. The BLM reevaluated the previous Decision Record from 2010 and granted a Determination of NEPA Adequacy on 26 October 2022. The BLM requires that the existing tailings impoundments are closed at the start of facility operations. QLM removed over 300 tons of trash and scrap from the site. They also removed derelict office trailers, vehicles, and equipment. The southwestern portion of the property was reclaimed and graded with excess material placed on the historical tailings to the northwest as initial cover material.

Processing: The expected mill life is 5 years from the start of construction development to the initiation of final reclamation. Mill life could be extended if exploration efforts at the ore source mine sites identify additional resources for the milling operation. The milling schedule is based on a daily throughput maximum of 200 tons of ore. The Operator may source ore from other permitted facilities within Nevada or from out of State facilities with prior approval from the Division based on ore characteristics.

The Red Rock Mill is estimated to run 200 tons per day (tpd) in a mill setting that can operate a gravity concentrating circuit followed by flotation plant. Mill feed will be sourced from a Division permitted mine facility. Ore will be hauled by highway trucks from the mine source to the site ore stockpile, then transferred to a primary jaw crusher. From the jaw crusher, the material will be conveyed to a secondary cone crusher; thence the material will be screened to minus 3/8 inch and dropped into a fine ore bin. The plus 3/8 material will be transferred back to the cone crusher for additional crushing. Material from the fine ore bin will then transfer to inside the mill building via the ball mill feed conveyor, which also will include a weigh scale. Once inside the mill building, ore from the ball mill feed conveyor will drop into the grinding mill, with the finely ground material (80% -200 mesh) exiting into the mill discharge sump. The ground ore material will enter a gravity concentrator feed pump for delivery to the gravity concentrator. Thence,

the material will be gravity sorted for transfer to either the concentrating table for production of a mineral concentrate or to a cyclone feed directing the material back to the cyclone classifier, which will direct the material to the flotation circuit, which will consist of two parallel flotation circuits. Feed from the cyclone classifier will enter two parallel flotation conditioners for preparation of the material to enter the rougher flotation circuits. Float material from the rougher flotation circuits will advance to the cleaner flotation circuits while the remaining tailing material and solutions are piped to the Tailings Storage Facility (TSF). Float material in the cleaner flotation circuits will advance to the concentration dewatering circuit, while excess water solutions will transfer back to the flotation conditioner. Concentrate from the cleaner flotation circuits will advance to the final concentrate thickener, then be pumped to a series of agitator tanks; thence, the material will advance to a filter feed pump that will deliver the concentrate to a concentrate filter, which will separate the final filtered concentrate product. Water from the concentrate filter will be piped to the TSF where it will be decanted and piped back to the flotation plant as make-up water. Concentrates from the gravity and flotation circuits will be transferred separately into super sacks for transport off site for final processing and refining at a Nevada permitted or out of State facility.

Reagents and Chemicals: Flotation agents will be supplied in 42-gallon barrels that will be stored in the Mill Building on the curbed concrete floor. There are only two plant flotation reagents that will be used in the beneficiation process: Aerophine 3418 and Flottec F145LV. Hydrocarbon products, including lubricants and oils, and antifreeze will be stored at the Maintenance Shop. These reagents and other chemicals will be transported, stored, and used in accordance with federal, state, and local regulations. All reagents and chemicals will be managed consistent with the Spill Prevention, Control, and Countermeasure (SPCC) Plan developed for the Project. Additional chemicals including dust suppressant surfactants and herbicides for noxious weed control will not be stored in the Project Area.

Mill Water Supply: Milling operations will require an estimated steady-state water flow of 147 gallons per minute (gpm). Make-up water requirement from the on-site well is estimated to be 23 gpm, while the recycled water requirement is estimated to be approximately 13 gpm. Most of the water delivered for the milling operation will be supplied by decanted water in the TSF via the Recycle Water Pipeline. Makeup water requirements will vary due to seasonal evaporation of recycled water in the TSF.

Mill Containment: The refurbished curbed concrete mill floor is designed to contain 115 percent of the volume of the largest vessel, exceeding the required 110 percent containment capacity for the largest vessel. The largest vessel to be utilized inside the mill building is the Reclaim water tank at 785 cubic feet, nearly 6,000 gallons. The total containment capacity of the mill building is 6,907 gallons. Any fluid leakage will flow to a floor sump at the west end of the building, where it will be pumped back to the beneficiation circuit or pumped into an active TSF pond.

The Mill Process Building floor will be refinished with a minimum of 1 inch of new concrete floor overlay over the existing concrete slab and concrete curbs around the exterior of the floor. The new curbs will be doweled into the existing concrete slab with retrofit waterstops around the perimeter. The curbed concrete floor will be sloped toward a new floor sump located at the west end of the building. Clean water that accumulates in the floor sump will be pumped back to the milling circuit. If the water in the sump has been contaminated with oil or grease, a portable pump will be used to fill a portable tank for delivery to an offsite facility for proper disposal. A two-part epoxy, or equivalent, will be used if cracks in the concrete are identified following construction and during operations. The epoxy will also be applied to areas where the new floor covering contacts existing building and equipment supports.

Tailings Management: Slurry solutions containing tailings generated from the mill will be conveyed to the TSF consisting of 4 ponds. Initially, the tailing from the mill will report to TSF Pond 1. As the tailing solids and decanted water volume capacity of TSF 1 nears full capacity, the bottom of freeboard elevation, tailing deposition will commence to TSF Pond 2. Once TSF Pond 1 has reached full capacity, tailing slurry deposition in the pond will cease. Tailing slurry deposition will advance in the same manner sequentially to TSF Pond 3 and TSF Pond 4. Once TSF Pond 4 has reached full capacity, the milling operation and generation of tailings will cease. As each pond reaches its solids capacity, the remaining freeboard volume will be filled with soil and covered with growth media such that it is free draining preventing runoff contributions to down gradient TSFs.

The TSF is designed as a zero-discharge facility. The ponds are designed for containment of excess solution which may result from a fluid spill in the Mill Building or precipitation from storm events. Spills in the mill building will only be transferred to a TSF if there is adequate capacity below the 2-foot freeboard level for the volume of the spill. The TSF is sized to contain the direct precipitation of the 100-yr 24-hr storm event plus 2 feet (ft) of freeboard. The volume of each TSF pond is based on the total volume of tailing solids and fluids that will occupy the pond below 2 feet of freeboard. As water separates from the tailing slurry in the TSF pond, it will decant to the surface of the pond and be pumped back to the mill as recycled water for reintroduction into the beneficiation process.

TSF Ponds 1, 2 and 3 will be approximately 200 feet wide by 334 feet long at their rims. TSF Pond 4 will be approximately 137 feet wide and 306 feet long. The ponds will be approximately 20 feet deep, including 2 feet of freeboard, with 2.5 horizontal to 1 vertical (2.5H:1V) side slopes. The top of freeboard elevation will be the bottom of the Pipe Channels, which are 1 foot below the pond rims, in each TSF pond. Each pond will be double lined with 60-mil High Density Polyethylene (HDPE) MicroSpike liners prior to placement of mill tailings. A synthetic GeoNet drainage layer will be installed between the two HDPE liners to facilitate leak detection in the event of a leak in the primary HDPE liner.

An alternative to the installation of a GeoNet drainage layer will be the substitution of the 60-mil textured MicroSpike HDPE primary liner with 60-mil double sided textured and dimpled MicroDrain HDPE liner. This would eliminate the need for the 200-mil GeoNet drainage layer since the dimpled liner would meet the drainage requirement.

Leak detection methods have been incorporated into each TSF pond. Leakage through the primary liner will flow between liners along a 200-mil GeoNet layer placed between the primary and secondary geomembranes, or along the drainage space provided by a MicroDrain primary liner to the leak detection and collection sump. The leak detection sump will be placed between the 60-mil textured HDPE geomembrane liner and the 60-mil textured HDPE geomembrane secondary liner in the pond. The sump system in the TSF ponds consists of 3/4-inch gravel wrapped in 12-oz geotextile adjacent to 6-inch diameter perforated PVC monitoring pipes. A piezometer will be installed in the monitoring pipe to measure the level of collected seepage, if any. From the sump, any collected solution can be removed via submersible pumps that will reside in the perforated PVC monitor pipe placed in the leak detection sump. From the submersible pump's discharge hose, any collected solution can be tested and pumped back into the pond or into an alternate TSF pond, if necessary.

Solution Pipeline Channels: Solution Pipeline Channels (SPC) at the Project consist of one Main Pipe Channel, four Tailing Pipe Notch Channels, four Recycle Pipe Notch Channels, and three Inter-Pond Pipe Channels. Each SPC will consist of a 60-mil HDPE lined open channel in which the solution conveyance pipelines will occupy. Any leak emanating from a pipeline will be contained by the HDPE liner and will flow by gravity to the TSF. The presence of solutions on the liner will alert personnel at the site in the event of solution leak in a pipeline. The liner system of all SPCs will be comprised from the bottom up of prepared subgrade, a minimum 1-foot-thick compacted soil layer overlain by a textured 60-mil HDPE liner.

Ore Stockpile facility: The existing concrete stockpile pad will be demolished and removed from the site or broken in place and buried by a minimum of 3 feet of growth medium. A third alternative may be to bury within the footprint of the reclaimed tailings following demolition. Prior to burial of concrete foundations or any other solid waste the Permittee will attain from the Bureau of Sustainable Materials Management (BSMM) a Class II Landfill Permit or waiver.

A new Ore Stockpile Facility (OSF) will be constructed near the mill crusher circuit. Run-of-mine ore will be delivered by highway trucks to the OSF. Ore transported from the off-site mining area will be temporarily stored at the OSF. The OSF will be loaded by end dumping the ore onto the footprint of the reinforced concrete stockpile, which includes 4-foot-high reinforced concrete stem walls along the back and sides. Stockpiled ore will be transferred by a loader to the crushing circuit. The OSF containment design will be comprised from the bottom up of prepared subgrade, a minimum 1-foot-thick compacted soil layer overlain by a minimum 5-inch Type 2 Class B aggregate then topped with an 8-inch reinforced

(#6 Bars on 6-inch centers), 4,000 pound per square inch concrete slab. The aggregate base shall be moisture conditioned to within 2 percent of optimum moisture content, placed in 6-inch maximum loose lifts and compacted to a minimum of 95 percent of maximum dry density (American Society for Testing and Materials (ASTM) Method D-1557).

Any meteoric water accumulations that may occur within the OSF will be contained within the concrete floor and stem walls and will drain to the north corner of the structure. The TSF will be used as a repository for any meteoric water that may accumulate in the OSF. Accumulated meteoric water will only be transferred to a TSF if there is adequate capacity below the 2-foot freeboard level for the volume accumulated meteoric water. The environmental technician will inspect the stockpile following significant storm events. If appreciable water (enough to pump) has accumulated in the stockpile, a portable pump will be used to fill a portable tank for delivery to the TSF ponds, where the pump will transfer the water to the TSF ponds.

Storm Water Diversion: The mill site is located within Soda Springs Valley. Geomorphologically, the site is located at the base of an alluvial fan, immediately upgradient of an alkali flat. The drainage basin upgradient from the mill site encompasses a total of 295 acres of alluvial terrain. The upgradient watershed is further divided into two subbasins: the North Basin (166 acres) and the South Basin (128 acres). The typical soil profile is characterized by extremely gravelly loamy sand on the surface and stratified extremely gravelly coarse sand to gravelly loamy sand with a very low runoff class. The extreme lower portion of the South Basin consists of a top surface of silt loam with silty clay loam in the deeper soil horizon (Natural Resources Conservation Service Web Soil Survey).

The upgradient watershed, originating in upgradient alluvial soils, was delineated for estimation of the potential 100-year and 500-year, 24-hour storm event flow rates. Peak flows were calculated, utilizing HEC-HMS modelling software with inputs of NOAA Atlas 14 Point Precipitation Frequency Estimates, soil characteristics, and vegetative type and cover. The portion of the alluvial fan immediately upslope from the Project site is calculated to convey a peak flow rate of 1.4 cubic feet per second (cfs) for the 100-year, 24-hour storm event and 3.5 cfs for the 500-year storm event. Stormwater flow will be managed by v-ditch drainage channels constructed on the perimeter of the Project site and the interior of the site. The perimeter v-ditches are designed to channel the off-site storm event water flows around the outside of the Project area. The interior v-ditches will channel the on-site water stormwater flows away from the TSF ponds and discharge the water downgradient of the site.

Protection of the Project site from potential off-site water run-on will be accomplished by diverting the flow from the upgradient watershed around the Project area via v-ditch channels located between the property boundary and existing road along the east side of the site. The perimeter ditch was designed to protect the project site from the worst-case scenario storm event (500-year, 24-hour

occurrence) located along the eastern boundary of the mill site. However, there is little visual evidence of storm water flow at the mill site and immediately upgradient of the Project site.

Process and Make-up water will be provided by the on-site well at the Red Rock Mill site. Water quality data from the existing on-site well was collected and sampled on 16 April 2009. The Permittee collected a water sample from the domestic well on 7 March 2023. The results indicate the sample met all Profile I drinking water standards. Depth to groundwater from top of casing was 105.3 feet.

Existing Historical Tailings: Tailings in the existing ponds are the result of previous milling activities. Samples of the existing tailings were collected, and Meteoric Water Mobility Procedure (MWMP) lab tests were performed to evaluate baseline conditions. The Purpose of the MWMP analysis is to evaluate the potential for dissolution and mobility of certain constituents from rock samples by meteoric water. The results can be used to assess soluble and insoluble contaminants, which could potentially be produced from the mill tailings and potentially migrate to the groundwater over time.

A total of 17 samples were collected from the existing tailings facility to test the material for its Acid Neutralization Potential and Acid Generating Potential (ANP/AGP). The method of testing was the Modified Sobek Acid Base Accounting (ABA) procedure. Each sample was a composite sample associated with each tailings cell.

Analytical results from the ABA testing for the existing tailings facility were compiled and evaluated. The results indicate that tailings materials exhibit very low AGP and possess a very strong or high ANP. The ration of neutralization potential for acidification potential was high as 2000:1, which far exceeds the minimum ratio of 1.2:1. The ANP/AGP ratios generally range from approximately 9.1 to >2000:1 with one [TP11] at 1:10, which greatly reduces the risk of developing conditions that would leach metal from these existing materials in the future. The results of the pH analysis indicate the tailings range from 8.83 to 9.53 standard units.

Analytical results from the Toxicity Characteristic Leaching Procedure (TCLP) for the existing tailings facility were collected. The TCLP analyzed each sample for the presence of the eight Resource Conservation and Recovery Act (RCRA) metals. These eight metals and their levels, in a specific material, determine if a material qualifies as a hazardous waste under the Federal Resource Conservation and Recovery Act. Only one sample came back above a the TCLP standard. Sample TS-2 contained lead at 12 mg/l and the standard is 5 mg/l.

The current plan to cap the tailings was previously approved by the BLM as a part of the projects approved plan of operations. Reclamation of the existing 5.4-acre tailings impoundment area will be completed before development of future tailings impoundments areas. As the new tailings ponds are excavated the historical ponds will be capped with the excavated material.

Ore Characterization: The Permittee completed multi-element ICP, MWMP, X-Ray Fluorescence , ABA, and Net Acid Generation (NAG) test work on ore material from the Goldfield Bonanza Mine, NEV2017109, which will provide ore feed to the Red Rock Mill. Rock characterization testing is not available for the tailing stream from the flotation circuit. However, the gravity and flotation circuits will remove most metals, which will render the tailings relatively inert. The double HDPE-lined and leak detection equipped TSF will fully contain any chemicals of potential concern.

Ancillary Facilities: Electric Power: Power will be supplied by an overhead power line. No backup generator will be required for operations at the facility.

Fuel Storage: A fuel storage facility will be located north of the mill in the mill yard area. One 1,000-gallon diesel tank and one 500-gallon gasoline tank will be situated atop a 60-mil HDPE lined containment basin. The basin will be encircled by a 1-foot-high berm which will provide 110 percent containment of the 1,000-gallon tank.

Maintenance Shop: An existing 85 ft by 35 ft maintenance shop is located north of the Mill building. Hydrocarbon products, including lubricants and oils, and antifreeze will be stored at the Maintenance Shop in either double walled vessels or on containment pallets.

PCS Plan: Any project petroleum contaminated soil will be properly containerized and transported offsite for proper disposal.

Assay Lab: The Assay Lab will be housed in separate rooms in the Maintenance Shop. A new Class II Air Quality Operating Permit and Mercury de minimus application authorizing operations at the Assay Lab will be in hand before any assay operations commence. The lab will be equipped for fire assay, atomic absorption analysis and flotation testing. The lab will include a collection sink for spent chemicals and lab equipment cleaning. The sink drain will report to a 500-gallon tote outside the lab building. The tote will be taken to an operating tailings pond and drained into the tailings pond if the contents meet the TCLP criteria. Otherwise, the contents will be disposed of off-site at an appropriate receiving facility.

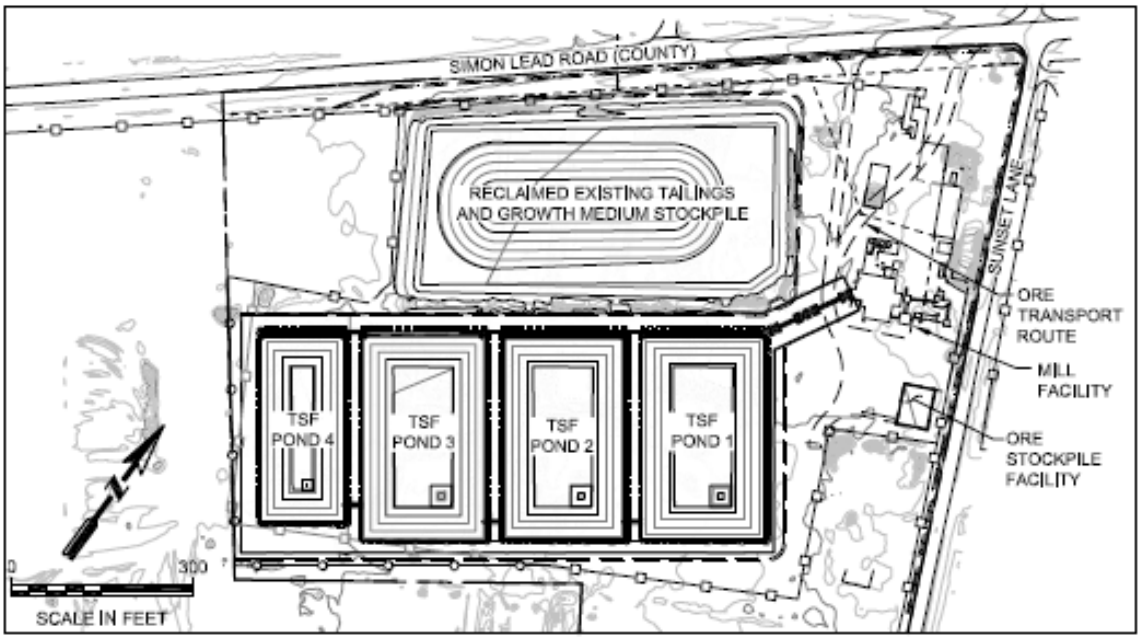
Security Office: A Security Office will be located at the fence gate at the entrance to the Project site.

Fencing: Approximately 3,774 linear feet of chain-link fencing currently encircles the Project facilities. 930 linear feet of the fencing will be removed in the TSF Pond 4 area to provide maintenance access to the pond. The segment of fence will be replaced with approximately 1,040 linear feet of a new chain-link fence.

Water Supply: Water for the milling operation will be sourced from the site Domestic water well and recycled water pumped from the TSF. Recycled water will be stored in two water tanks, each with a capacity of 6,000 gallons, inside the Mill building. A 14,500-gallon water tank located in the crushing area outside the mill will be used for storage of water from the domestic well only. No recycled

water from the TSF will be stored in the tank. The tank will provide makeup freshwater storage for milling operations and dust suppression water for the site.

General Facilities Arrangement



MILL AND TAILING FACILITY

C. Receiving Water Characteristics

The Project is located within the Nevada Department of Conservation & Natural Resources- Division of Water Resources (NDWR) Hydrographic Region number 10 (Central Region), Administrative Groundwater Basin 121A (Soda Spring Valley-Eastern Part). Groundwater Basin 121A is classified by NDWR as "Designated-Irrigation Denied". The Soda Spring Valley is a closed basin. Groundwater Basin 121A is typical of arid drainage basins in Central Nevada where precipitation is generally insufficient to support perennial stream flow. Small ephemeral channels begin in the higher elevations and convey water to the low valleys.

The Nevada Department of Water Resources, Nevada Hydrology Mapping Application was queried to identify drinking water wells within 5-miles of the site. The search identified 10 municipal and domestic wells within a 5-mile radius of the Project. All of the wells are located upgradient of the site including the domestic well located at the Project site just east of the mill building (Well Log 23942).

An existing well designated for mining and milling is located at the northeastern side of the Project area. The well was completed in 1969 to a depth of 248 feet below the ground surface (bgs). Based on Driller's Log #10839, the static water level was 100 feet bgs at the time it was drilled. The existing 12-inch diameter well

does not have sanitary seal and will be plugged and abandoned following requirements of NAC 534.420.

Based on the domestic (Well Log 23942) groundwater depth was 46 feet bgs at the time of drilling. The existing 8-inch diameter on-site well has a concrete slurry sanitary seal installed to 50-feet below the ground surface as required by Nevada water well regulations. The well was drilled to 265 feet bgs. The domestic well groundwater depth was checked by the Permittee's staff on 7 March 2023. At that time the groundwater depth was noted as 105.3 feet from top of casing. Groundwater sampling results indicate the water meets all Division Profile I drinking water standards.

Two wells will be used for groundwater monitoring at the site. An existing eight-inch diameter, 265 ft bgs deep production water well (PW-1) located in the mill yard area will be used for upgradient groundwater monitoring in addition to supplying fresh makeup water for milling operations. A new monitoring well (MW-1) will be constructed west of TSF Pond 4 to monitor groundwater down gradient of the site.

There are no streams or springs within one mile of the Project. With the exception of the alkali flat (playa), which occasionally ponds surface water after precipitation events, there are no features that could be considered surface water within a 1-mile radius of the project site. All surface waterways within 1-mile of the facility are ephemeral and flow only during precipitation events.

The Potential Evapotranspiration Evaporation estimate for the Dead Camel Mountain RAWS Station adjusted to the Red Rock Mill site elevation is 69.75 inches annually. The mean annual precipitation is 4.52 inches per year.

D. Procedures for Public Comment

The Notice of the Division's intent to issue a Permit authorizing the facility to construct, operate and close, subject to the conditions within the Permit, is being published on the Division website: https://ndep.nv.gov/posts/category/land. The Notice is being mailed to interested persons on the Bureau of Mining Regulation and Reclamation mailing list. Anyone wishing to comment on the proposed Permit can do so in writing within a period of 30 days following the date the public notice is posted to the Division website. The comment period can be extended at the discretion of the Administrator. All written comments received during the comment period will be retained and considered in the final determination.

A public hearing on the proposed determination can be requested by the applicant, any affected State or intrastate agency, or any interested agency, person or group of persons. The request must be filed within the comment period and must indicate the interest of the person filing the request and the reasons why a hearing is warranted.

Any public hearing determined by the Administrator to be held must be conducted in the geographical area of the proposed discharge or any other area the

Administrator determines to be appropriate. All public hearings must be conducted in accordance with NAC 445A.403 through NAC 445A.406.

E. Proposed Determination

The Division has made the determination to issue the new Permit.

F. Proposed Limitations, Schedule of Compliance, Monitoring, and Special Conditions

See Section I of the Permit.

G. Rationale for Permit Requirements

The facility is located in an area where annual evaporation is greater than annual precipitation. Therefore, it must operate under a standard of performance which authorizes no discharge(s) except for those accumulations resulting from a storm event beyond that required by design for containment.

The primary method for identification of escaping process solution will be placed on required routine monitoring of leak detection systems as well as routinely sampling the downgradient monitoring well. Specific monitoring requirements can be found in the Water Pollution Control Permit.

H. Federal Migratory Bird Treaty Act

Under the Federal Migratory Bird Treaty Act, 16 U.S. Code 701-718, it is unlawful to kill migratory birds without license or permit, and no permits are issued to take migratory birds using toxic ponds. The Federal list of migratory birds (50 Code of Federal Regulations 10, 15 April 1985) includes nearly every bird species found in the State of Nevada. The U.S. Fish and Wildlife Service (the Service) is authorized to enforce the prevention of migratory bird mortalities at ponds and tailings impoundments. Compliance with State permits may not be adequate to ensure protection of migratory birds for compliance with provisions of Federal statutes to protect wildlife.

Open waters attract migratory waterfowl and other avian species. High mortality rates of birds have resulted from contact with toxic ponds at operations utilizing toxic substances. The Service is aware of two approaches that are available to prevent migratory bird mortality: 1) physical isolation of toxic water bodies through barriers (e.g., by covering with netting), and 2) chemical detoxification. These approaches may be facilitated by minimizing the extent of the toxic water. Methods which attempt to make uncovered ponds unattractive to wildlife are not always effective. Contact the U.S. Fish and Wildlife Service at 2800 Cottage Way, Room W-2606, Sacramento, California 95825, (916) 414-6464, for additional information.

Prepared by: Shawn Gooch, P.E.
Date: 10 July 2023

Revision 00: New Permit, effective **28 July 2023**.