FACT SHEET
(Pursuant to Nevada Administrative Code (NAC) 445A.401)

Permittee Name: **Quartz Lake Mining, Inc.**

Project Name: **Goldfield Bonanza Mine Project**

Permit Number: **NEV2017109**
Review Type/Year/Revision: **Renewal 2023, Fact Sheet Revision 00**

A. Location and General Description

Location: The Goldfield Bonanza Mine Project is located in east-central Esmeralda County, within portions of Sections 35 and 36, Township 2 South (T2S), Range 42 East (R42E); and Sections 1 and 2, T3S, R42E, Mount Diablo Baseline and Meridian, approximately 0.3 miles east of the town of Goldfield, Nevada. The Project is located on private land owned by Lode Star Gold, Inc (LSG). Quartz Lake Mining, Inc. (QLM) is the Permittee, and operator of the property.

The Project may be accessed by automobile, from Goldfield, by turning northeast onto North 5th Avenue from United States Route 95. Proceed northeast approximately 0.6 miles on North 5th Avenue to where the office building is located.

General Description: The Project consists of an underground mine accessed by the rehabilitated February-Premier Shaft. The existing mine and new workings will be utilized to access the proposed mining zones that will be mined utilizing narrow vein extraction techniques. Ore will be extracted, and additional exploration drilling will be performed to determine the economics and feasibility of continued future operations. Ore will be shipped off-site to a Division-permitted or out-of-state facility for final processing. There is no on-site crushing or processing and no dewatering of the underground workings are proposed at this time. The 2023 Major Modification and Renewal allows for the transitioning of the mine as an exploration activity permitted under 445A.415 to become a fully operating mine permitted under 445A.394. The major modification includes the installation of a 100,000-ton High Density Polyethylene (HDPE) lined Waste Rock Facility (WRF), a 1,000-ton concrete lined Ore Stockpile Facility (OSF2). Production increase from 4,000 tons of ore to 99,900 tons of ore per year. Additional monitoring and characterization for long term planning. Expanded mining below the 300 level while remaining above the existing groundwater level.

B. Synopsis

Geology: The Lode-Star property is located along the southwestern margin of the Goldfield ring fracture zone, an area of very strong alteration fracturing and faulting generally in the north-northwest and northeast directions. The oldest geologic unit in the area is the Ordovician Palmetto Formation, which consists primarily of fine grained clastic sediments, including local calcareous sediments. The principle host rocks of the property and the Main District are andesitic flows of the Milltown

Andesite and a large dacite porphyry intrusive body. These are overlain by post-mineral coarse clastic sediments of the Siebert Formation.

Float gold was discovered in the western Goldfield Hills in 1902 and mining of the siliceous veins began in late 1903. Within a few years, the population of Goldfield expanded to approximately 25,000 people, with production reaching a peak in 1910. At peak production, the Goldfield deposit produced approximately 16.8 tons of gold and 3.67 tons of silver per year. The first production was of high grades from the Phelan shaft in the northern part in 1910. Other modest production was made from several shafts on the property. The first significant production was made by Newmont Mining in 1949-51 in the Newmont Lode and Red Hills areas.

The Lode-Star Mining, Inc. property was explored by Trafalgar Mines and Westley Mines from 1983 to 1988 a total of 37,000 feet were drilled and seismic studies of the property were performed. From 1988 to 1997 Geochem Mines explored the property further and rehabilitated the February-Premier shaft. Lode-Star Mining, Inc. explored the property from 1998 to 2010 which included rehabilitation and sampling of old workings, and extensive surface and underground drilling. In March 2011, Lode-Star Mining, Inc. carried out an extensive exploration program.

In April of 2022, the Division approved a Permit transfer from Lode-Star Mining, Inc. to LSG. QLM optioned the property in January 2022 and became the operator. In July 2022 the Permit was transferred to Quartz Lake Mining, Inc., the current operator of the facility. LSG remains the facility landowner.

Mining: The main access to the Goldfield-Bonanza project is via the historical February-Premier Shaft, which has been rehabilitated and is open to approximately 300 feet below ground surface (ft bgs), also known as the 300-level. An additional shaft, the existing January-White Rock Shaft may be rehabilitated in the next few years, depending on exploration results. Existing and new mine workings will be used to access the proposed mining zone, which will be mined using narrow vein extraction techniques. Waste rock will be placed underground as lime amended backfill and into nearby existing, historical surface shafts on the property. Waste rock will also be placed without lime in the HDPE lined 100,000-ton Waste Rock Facility (WRF). Ore will be transported to the surface through the February-Premier Shaft, loaded onto trucks and transported off site for processing. Ore may also be placed in one of three locations for storage prior to shipment: OSF1 (described below), OSF2, or temporarily on the WRF as needed. Currently there are two areas, the Red Hills and the Church, that are incorporated in the mine plan. A third area known as the Newmont Lode to the south is also being investigated for mining potential.

All mining will be conducted above the water table. All workings in and above the mining zone are dry. No seepage or moisture has been observed in the workings down to the 370-level. Any future mining below the existing water table will require the submittal of a Permit modification to ensure that waters of the State are protected and may require the submittal of a permit application for a dewatering management facility.

Mining in the Red Hills area will extract ore from the currently exposed Stope Vein Zone, and the Decline Vein Zone down to the 370-level. Mining dimensions in the Stope Zone are expected to be an average of 4 to six 6 feet wide, approximately 60 feet upwards and 80 feet along strike. Mining in the Decline will achieve ore extraction and development of access to lower levels while remaining above the water table. Eventually, the gold ore below the 370 level in both the Stope and Decline Vein Zones will be removed through deepening of the February-Premier shaft or the development of a downward spiral ramp, ultimately accessing mining depths of approximately 450 ft bgs. QLM has provided a mitigation strategy to allow for mining down to the existing water table in areas that may be inundated in the future. It has been determined that lime amended waste rock placed underground will mitigate future potential degradation by maintaining an adequate groundwater pH during any potential future mine inundation due to rising groundwater.

The currently identified high-grade gold ore in the Church area exists in a near-vertical zone extending essentially directly above the currently accessible 300-level down to the 370-level mine workings. There is also a known oxide zone that extends from the 100 level down to the 200 level. This zone is currently believed to be approximately 40 feet wide and 150 feet in vertical extent.

Ore material is to be stored underground as needed in muck bays while waiting for assays. Ore is transported underground with a 1-yard scoop-tram loader. From muck bays or directly from the working face. Ore is moved to surface via a 1-ton skip. On surface the ore is loaded into a truck utilizing a conveyor from the shaft loadout to minimize the materials exposure to meteoric water. The existing exploration hoist at the February Premier shaft will be replaced with a larger production hoist and 2-ton bucket.

To avoid temporarily shutting down while a Major Modification for expansion is being prepared, the Division approved (on 26 January 2022) of a proposal to substitute 6,000 tons of permitted ore tonnage for 6,000 tons of waste tonnage to facilitate the construction of a secondary escape way and remain compliant with the MSHA 2009 guidance regarding escapeways and refuges. The Permit originally required that no more than 10,000 tons of ore and 1,400 tons of waste be generated by the project prior to the Divisions approval of a Major Modification for expansion beyond these limits. The revised tonnage allowed for the permitted production of 4,400 tons of ore and 7,000 tons of waste.

Interim Waste Rock Management Plan: An Engineering Design Change (EDC), was submitted 21 February 2023 for an Interim Waste Rock Management Plan and was approved by the Division in April 2023. The EDC allows for alternative surface waste rock disposal in the event that the mine ran out of available waste rock storage space in the approved backfill shafts prior to the approval of the 2023 Major Modification and renewal. The plan requests disposal of up to 5 feet of lime amended waste rock on 4 select historical sulfide dumps. The material would then be covered with a minimum of 3 feet of select overburden and then seeded for final

reclamation. This plan allows the mine continuous operations while closing the historical waste rock Facilities.

The Project plans to mine approximately 99,900 tons of ore per year at a rate of approximately 270 tons per day. The Project life is estimated at 5 years. Ore material will be shipped off-site to either a Nevada Permitted facility or an out of state facility for processing. Any increases in production would require the submittal and written Division approval of a Major Modification pursuant to Nevada Administrative Code 445A.394.

Ore Stockpile Facility 1 (OSF1): On 17 August 2022 the Division approved an Engineered Design Change to install a 1,000-ton HDPE lined OSF. In order to efficiently fill over the road trucks, the Permittee constructed a surface ore stockpile pad. The ore stockpile pad allows for the storage of approximately 1,000 tons of ore on the surface and decreases truck loading times by removing the current need to hoist ore from the underground workings directly into the bed of a truck. The OSF1 EDC was originally submitted as a temporary stockpile however the Division considered the "temporary ore stockpile pad" as an "ore stockpile pad" since it meets the design requirements for longer term ore storage.

The stockpile pad is rectangular in shape, approximate dimensions of 71 feet by 88 feet, and is synthetically lined with a smooth 80-mil high-density polyethylene liner to provide for watertight containment. Prior to beginning preliminary grading, the area was cleared and grubbed. The soil was moisture conditioned and smooth drum rolled then visually inspected to remove all rocks and possible protrusions. The compacted fill was moisture conditioned to within 2 percent of optimum moisture content, placed in 12-inch maximum loose lifts and compacted to a minimum of 90 percent of maximum dry density (ASTM D-1557). Perimeter berms measuring 4 feet in height are utilized to provide containment of the water resultant from a 500-year, 24-hour storm event that contacts the ore materials and to prevent run-on. The pad is sloped at a minimum of 1% to the northern corner to allow for the collection and removal of solutions, which will be sent to an appropriate facility if needed. A 2-foot lift of overliner consisting of -2" fine grained high clay content low grade ore was placed prior to depositing high grade ore. The subgrade and overliner materials are designed to be protective of the liner and provide a firm unyielding surface and promote drainage, respectively.

Run-of-mine (ROM) ore will be delivered by an 8-ton dump truck to the Ore Stockpile Facility (OSF1) adjacent to the haul road. Ore transported from the mining area will be temporarily stored at the OSF1. The ore stockpile will be loaded by end dumping the ore onto the footprint of the HDPE lined stockpile, which includes 4-foot-high HDPE lined berms. Stockpiled ore will be loaded by a loader onto highway trucks for transport to off-site processing facilities.

Ore Stockpile Facility 2 (OSF2): In addition to the HDPE lined OSF 1 the 2023 Major Modification and Renewal includes the construction and operation of a second ore stockpile ,OSF 2, that will be concrete lined. OSF2 is located 480 feet northwest of the February-Premier Shaft. The OSF2 will be concrete lined over an

area of 51 x 68-feet, with concrete stem walls measuring 4 feet high. Following clearing and grubbing, an aggregate base shall be placed as the base surface for the OSF concrete slab, footings, and fill slopes. The concrete floor slab and stem walls will be constructed over a minimum of 5 inches of Type 2 Class B crushed and compacted aggregate base. The aggregate base shall be moisture conditioned to within 2 percent of optimum moisture content, placed in 6-inch maximum loose lifts and compacted to a minimum of 95 percent of maximum dry density (ASTM D-1557). At all concrete construction joints water stops (Sika® Greenstreak® (PVC) waterstops 6" flat ribbed) will be installed. The floor of the facility will be a single continuous slab. Contraction/control joints will be installed on the floor slab 1" deep on 20-foot centers. Those joints will be filled with epoxy.

Run-of-mine (ROM) ore will be delivered by an 8-ton dump truck to the Ore Stockpile Facility (OSF2) adjacent to the haul road. Ore transported from the mining area will be temporarily stored at the OSF2. The ore stockpile will be loaded by end dumping the ore onto the footprint of the reinforced concrete stockpile, which includes 4-foot-high reinforced concrete stem walls. Stockpiled ore will be loaded by a loader onto highway trucks for transport to off-site processing facilities.

Waste Rock Management: The Project will utilize three methods for placement of the waste rock generated from the Project: underground stope backfill, surface shaft backfill, and deposition on the WRF. Underground and surface waste rock backfill will be neutralized, utilizing quick lime, to an Acid Neutralizing Potential/Acid Generation Potential (ANP/AGP) ratio of 1.1 (to control metal leaching at higher pH) and stored in existing underground drifts, which are not subject to future mining, and within surface shafts present from historical mining in the Goldfield District. Surface deposition of waste rock on the HDPE lined WRF will not be Lime amended.

Underground stope backfill: Waste rock will be transported from the working face by loaders to the waste storage drift and placed as lime amended backfill. All areas identified for potential waste rock storage are also above the groundwater level, are dry and are predicted to remain so throughout mining.

Surface Shaft Waste Backfill Management: The Permittee, in conjunction with the Nevada Division of Minerals (NDOM), has investigated the potential of using 11 surface shafts for waste rock storage. All shafts are above the regional water table and are dry and deemed suitable for waste storage.

Waste rock will be hauled and brought to the surface in such a way that the waste rock will never be stockpiled above ground. The waste rock will be stored in dry muck bays underground and be brought in stages to the surface once a sufficient volume is available to backfill the shafts. This will ensure that a shaft is not left partially filled during backfilling.

At the top of the shaft a conveyor belt will then feed the waste rock from underground workings to a dump truck which will then transport the material to the selected shaft sites. The waste rock is end dumped from the dump truck directly

into the selected shafts for backfill. The actual lime mixture ratio will be affected by the type of alkaline material selected during operations. As the required mixture ratio is established for each area through the sampling and testing process, a standard mixture ratio will be established and used for the waste rock generated in each of the areas.

After completion of mining activities, or once a shaft's capacity is reached and the waste rock has settled, the shaft will have a closure cover placed over the opening. The closure cover consists of a synthetic liner and general fill placed in a manner to promote runoff of meteoric water, a 3-foot-thick low permeability soil layer (1×10^{-6} centimeters per second [cm/s]), and 3 feet of topsoil. The waste rock placed within the shaft will be allowed to settle and be monitored prior to placing the closure cover. Waste rock will be backfilled into the shaft during the settling period keeping the waste rock within 1.5 feet of the shaft's rim. Once settling of the waste rock has ceased or subsided, the shaft's closure cover will be placed. The closure cover will be constructed to account for any additional settling. The piece of synthetic liner and 3 feet of topsoil will protect the low permeability layer from freezing and thawing, ensuring no preferential flow paths are created in the low-permeability layer. Permanent fencing will then be placed surrounding the backfilled shafts to mark and identify the locations.

Once the material has been amended, quarterly samples will be collected and undergo Meteoric Water Mobility Procedure (MWMP) testing for Profile I constituent release and ANP/AGP testing. Results of testing will drive any modifications to the waste rock management process to maintain effective acid neutralization of the waste rock. Once the adequate mixture ratio is achieved, the amended waste rock will then be hauled to the drift or surface shaft for final storage. The alkaline buffer material will be brought from an offsite source and will consist of 2-inch minus graded quick lime or other crushed alkaline material.

On 26 August 2021, the Division approved the addition of the North and South Shafts to the backfilling regimen. The shafts have rough surface areas of 728 and 1,911 square feet, respectively, and are anticipated to provide approximately 2,772 tons of storage capacity. This results in a total shaft capacity of approximately 6,926 tons. The waste material will be amended, placed, and shafts closed as described above and required by the Permit.

Waste Rock Facility (WRF): The 2023 Major Modification and Renewal included the installation of a 100,000-ton WRF. The WRF will be used for the disposal of untreated underground waste rock placed on 100% HDPE lined containment with associated Storm Event Pond (SEP) for storm water management and full containment. The WRF may be utilized for temporary ore storage for both low grade and mill grade ores as needed. The WRF location was selected to minimize disturbed acreage and haulage distance. Topsoil suitable for growth medium will be removed from the facility footprint during construction and placed in stockpiles for use in final reclamation. The WRF is designed as a zero-discharge facility. The SEP is sized to contain runoff from the WRF, and locally surrounding upgradient

catchment areas during the 100-yr 24-hr storm event. Sizing of the pond did not consider stormwater retention by the dry waste rock stacked on the facility. It is a conservative design assuming all precipitation reports to the pond during the event. Generally, the facility will be dry with no drain down or fluid recirculation during operations and following closure at the site.

The WRF will be constructed from bottom to top with the following: a prepared subgrade, an 80-mil high density polyethylene (HDPE) liner, and 12 inches of overliner. The prepared subgrade will be constructed using compacted fill moisture conditioned to within 2 percent of optimum moisture content, placed in 12-inch maximum loose lifts and compacted to a minimum of 90 percent of maximum dry density (ASTM D-1557). The WRF overliner shall consist of excavated material from the Borrow Area in the wash to the southwest of the WRF.

The Storm Event Pond composite-lined system will consist of the following components from bottom to top: prepared subgrade, a minimum one-foot-thick compacted Soil Layer overlain by a textured 60-mil HDPE secondary Geomembrane Liner, then an HDPE 200-mil geonet drainage layer, followed by a textured 80-mil HDPE primary liner. The pond capacity is 293,035 gal with a 332 gal leak detection sump.

The subgrade surface shall be smooth drum rolled to provide a uniform surface with no projections larger than 3/8 inch. Fine-grained soils shall be used to provide suitable material for bedding the HDPE 60-mil textured HDPE geomembrane secondary liner. The drainage layer 200 mil geogrid drainage net will drain to a leak detection sump. An 80- mil textured HDPE primary liner with the textured side up will be the top surface.

Seismic Stability Analysis: A schedule of compliance item for the 2023 Major Modification and Renewal requires a seismic stability analysis to be performed prior to placement of the second 10-foot lift on the WRF.

WRF stormwater diversion: Surface water runoff from the upgradient drainage basin will be routed around the WRF through the Stormwater Diversion Channel. The Stormwater Diversion Channel will begin at the southwest corner of the WRF and extend around to the southeast corner then along the eastern side of the WRF all the way to the northeast corner where it directs surface water flows to the north into an existing drainage.

The channel will be constructed to divert surface flows during storm events from entering the WRF. The drainage area totals 10.1 acres and consists of gentle sloping topography with a maximum slope of approximately 10 percent. This channel will be constructed to divert a 500-year, 24-hour precipitation event (3.73 in.) around the WRF facility. The channel is small with a depth of 1.0 ft and a bottom width of 1 ft. and will have 2.5H to 1V side slopes. The maximum flow rate following the 500-year event is 11.9 cubic feet per second and will flow at a maximum depth in the channel of approximately 0.93 ft. To protect the higher channel side slopes from

erosion along the curve between 7+00 and 8+25 they will be over-excavated by 6" and a layer of 6" broken riprap will be installed.

Waste Rock and Ore Characterization: Two representative samples of waste rock from the underground workings were collected and analyzed for Profile I constituent release, utilizing an MWMP, and static testing, utilizing the Nevada Modified Sobek Procedure. Testing results displayed the waste rock had a high potential for acid generation with MWMP rinsate pH values of 2.68 and 2.42 and ANP/AGP ratios of less than 0.01. In addition, both Profile I analyses showed that the material has the ability to liberate aluminum, arsenic, beryllium, cadmium, copper, iron, magnesium, manganese, sulfate, total dissolved solids (TDS), and zinc above Profile I reference values.

Underground Waste Backfill Management: Due to the acid generation potential of the material, the Permittee proposed to amend the material with 2-inch minus graded quick lime or other crushed alkaline material at a sufficient ratio to obtain and ANP/AGP ratio of 1.2. The Division requested that, as part of the initial characterization report, amended samples be analyzed for Profile I constituent release by utilizing an MWMP procedure. The quick lime addition was added to splits of the originally collected samples in an amount that would produce an ANP/AGP ratio of 1.2. The amount of lime added was between 0.08 to 0.07 pounds of quick lime per pound of wasterock. The results of the testing displayed an increase in pH to 11.51 and 11.06 and a large reduction in leached metals with only aluminum (1.3 and 1.5 milligrams per liter [mg/L]), sulfate (1,900 and 2,600 mg/L), and TDS (2,800 and 3,500 mg/L), exceeding Profile I reference values. While the pH exceeds the Profile I reference value of 6.5 – 8.5, it has been determined as beneficial due to the additional buffering capacity the amended material will add to the backfilled underground workings in the event they become flooded in the future.

During review of the 2023 Major Modification/Renewal, the Division noted that elevated lead is being leached from the amended waste rock samples. Based on email discussion between the Division and the author of the geochemical report, this is most likely due to the elevated pH resulting from amending the materials to an Acid Neutralizing Potential to Acid Generating Potential ratio of 1.2.

The Division requires that the ANP/AGP ratio be lowered in an attempt to limit the leaching of lead, while still providing excess neutralization potential. The Division requires that an ANP/AGP ratio of 1.1 be utilized going forward.

Ancillary Facilities: Two diesel fuel storage tanks, each with a 5,000-gallon capacity, will be located by the office/yard area. Secondary containment will be in place for both tanks in accordance with NAC 445A.436. Additional fuels and oils will be stored in 55-gallon drums in the existing warehouse on pallets. Two generators containing fuel will be located at the entrance of the February-Premier Shaft. Above-ground facilities and equipment will be visually inspected on a regular basis for leaks, damage, or unusual conditions.

C. Receiving Water Characteristics

The Project is located in Esmeralda County within the Alkali Spring Valley Groundwater Basin (Hydrogeological Basin #142) as defined by the Nevada Division of Water Resources. The average groundwater recharge rate in the Goldfield area is generally low at approximately 5% of precipitation or approximately 0.33 inches per year based on an average annual precipitation rate of 6.5 inches. The average evaporation far exceeds the precipitation and ranges from approximately 51 to 72 inches annually. Groundwater generally has Division Profile I exceedances of sulfate (up to 1,600 mg/L), total dissolved solids (up to 2,700 mg/L), and manganese (up to 1.4 mg/L).

Groundwater in the vicinity of the Goldfield Bonanza Project is currently depressed due to the historic mining and subsequent dewatering of approximately 260 shafts in the early 1900's. It is estimated that some of the workings were dewatered to a depth of approximately 1,750 feet below the ground surface. Aquifer testing, consisting of pumping and slug testing, was performed on monitoring well 1 (MW-1) and MW-2. Hydraulic conductivity results for MW-1 ranged from $3.7x10^{-5}$ to $1.4x10^{-4}$ cm/sec and MW-2 ranged from $6.5x10^{-5}$ to $1.4x10^{-4}$ cm/sec, although the lower conductivity values are considered to be the most reliable due to the methodology of the testing performed. The low hydraulic conductivity values coupled with a low recharge rate explain why groundwater within the Project area is still depressed after 100 years since the cessation of dewatering in the area. It is anticipated that future dewatering and mining from proposed open pit mining in the area will continue to depress the groundwater levels for the life of the Goldfield Bonanza Project.

The Baseline Hydrogeology Report provided groundwater elevations from exploration boreholes, monitoring wells, surface shafts, and water elevations observed by staff. Groundwater depth in the project area measures from 317 feet to 434 feet below the ground surface. The proposed 370-level historical workings are dry and the underground workings will remain above the groundwater table during mining. There is anecdotal evidence from miners who accessed levels as deep as the 440-foot level that were dry as recently as 5 to 10 years ago. The mine intends to access these lower levels to determine the actual groundwater level in the immediate mine area.

The 2023 Major Modification and renewal requires a third monitoring well to be installed between the two existing monitor wells on the west side of the mine between the mine and town. Additional monitoring requirements for rock characterization over the next 3 years were determined for use in future groundwater modeling and planning for the potential to mine below the groundwater table should minable resource be discovered in the future.

Exploration borehole data from 1985 was compared with more recent groundwater elevations indicate that groundwater levels still appear to be rebounding slowly. It has not yet been determined what elevation the rebounding water table will rise to, but the pre-anthropogenic groundwater depth was reported as approximately 100 to 150 ft bgs in the vicinity of the Project. It is anticipated that future groundwater

pumping from the permitted mine to the north of the property may continue to drawdown ground water in the region, further delaying any groundwater rebound.

D. Procedures for Public Comment

The Notice of the Division's intent to issue a Permit authorizing the facility to construct, operate and close, subject to the conditions within the Permit, is being published on the Division website: https://ndep.nv.gov/posts/category/land. The Notice is being mailed to interested persons on the Bureau of Mining Regulation and Reclamation mailing list. Anyone wishing to comment on the proposed Permit can do so in writing within a period of 30 days following the date the public notice is posted to the Division website. The comment period can be extended at the discretion of the Administrator. All written comments received during the comment period will be retained and considered in the final determination.

A public hearing on the proposed determination can be requested by the applicant, any affected State or intrastate agency, or any interested agency, person or group of persons. The request must be filed within the comment period and must indicate the interest of the person filing the request and the reasons why a hearing is warranted.

Any public hearing determined by the Administrator to be held must be conducted in the geographical area of the proposed discharge or any other area the Administrator determines to be appropriate. All public hearings must be conducted in accordance with NAC 445A.403 through NAC 445A.406.

E. Proposed Determination

The Division has made the determination to issue the renewed Permit.

F. Proposed Limitations, Schedule of Compliance, Monitoring, and Special Conditions

See Section I of the Permit.

G. Rationale for Permit Requirements

The facility is located in an area where annual evaporation is greater than annual precipitation. Therefore, it must operate under a standard of performance which authorizes no discharge(s) except for those accumulations resulting from a storm event beyond that required by design for containment.

Specific monitoring requirements can be found in the Water Pollution Control Permit.

H. Federal Migratory Bird Treaty Act

Under the Federal Migratory Bird Treaty Act, 16 U.S. Code 701-718, it is unlawful to kill migratory birds without license or permit, and no permits are issued to take migratory birds using toxic ponds. The Federal list of migratory birds (50 Code of Federal Regulations 10, 15 April 1985) includes nearly every bird species found in the State of Nevada. The U.S. Fish and Wildlife Service is authorized to enforce the prevention of migratory bird mortalities at ponds and tailings impoundments.

Compliance with State permits may not be adequate to ensure protection of migratory birds for compliance with provisions of Federal statutes to protect wildlife.

Open waters attract migratory waterfowl and other avian species. High mortality rates of birds have resulted from contact with toxic ponds at operations utilizing toxic substances. The Service is aware of two approaches that are available to prevent migratory bird mortality: 1) physical isolation of toxic water bodies through barriers (e.g., by covering with netting), and 2) chemical detoxification. These approaches may be facilitated by minimizing the extent of the toxic water. Methods which attempt to make uncovered ponds unattractive to wildlife are not always effective. Contact the U.S. Fish and Wildlife Service at 1340 Financial Boulevard, Suite 234, Reno, Nevada 89502-7147, (775) 861-6300, for additional information.

Prepared by: Keith Johnson
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Revision 00: Major Modification/Renewal 2023 effective XX XXXX 2023, Transfer of Permit to QLM