

FACT SHEET
(Pursuant to Nevada Administrative Code [NAC] 445A.401)

Permittee Name: **Ruby Vista Resources Ltd.**

Project Name: **Gold Ribbon Mine**

Permit Number: **NEV2017106**

Review Type/Year/Revision **Renewal 2026, Fact Sheet Revision 00**

A. Location and General Description

Location: The Gold Ribbon Mine (GRM) is a small underground mine and physical separation facility, located in Pershing County, Nevada, approximately 20 miles northwest (by air) of the town of Imlay and 40 miles north (by air) of the town of Lovelock. The GRM is located within the LK#1 and LK#2 lode claims located on public land administered by the Bureau of Land Management (BLM) Winnemucca District—Humboldt River Field Office.

The GRM project site is located on the eastern flank of the Antelope Range and the western flank of the Majuba Mountains, within the historic Antelope Mining District (also referred to as the Cedar King and Majuba Hill mining districts). The Permittee (Ruby Vista Resources Ltd.) intends to process up to 18,000 tons of gold and silver bearing ore annually without the use of chemicals. Projected mine life is between one and five years.

The project site is located within portions of Section 18, Township 33 North, Range 31 East, Mount Diablo Baseline and Meridian.

Site Access: To access the GRM, proceed on Interstate-80 east from Lovelock or west from Winnemucca to *Exit 145—Imlay*. The town of Imlay is on the north side of the interstate. Proceed west on North Frontage Road a short distance to the intersection of Main Street. Turn north (right) onto Main Street and proceed 4 blocks to the intersection of Pacific Avenue. Turn west (left) onto Pacific Ave. and proceed approximately 0.9 miles to the junction of Frontage Road and Old Idaho Stage Road. Turn north (right) and proceed approximately 0.1 mile on Old Idaho Stage Road (crossing the railroad tracks) to the Y-junction of Lake Road and Flying M Ranch Road. Veer west (left) onto Lake Road and proceed 17.9 miles to the junction of Pioneer Road. Veer northwest onto Pioneer Road and proceed 4.5 miles to the junction with the unnamed mine access road (note some maps also refer to this road as Pioneer Road). Turn southwest (left) and proceed 1.7 miles to the GRM project site.

General Description: The proposed GRM is an underground mine with a physical separation facility on the surface. The mine is accessed through two inclined shafts (e.g., the Production Shaft and Ventilation/Escapeway Shaft) and mining will take place underground by drift development and stoping methods. Mined material will be delivered to the shaft station to load the production skip and hoisted out of the mine to the surface. The skip will dump into a bin on the surface. Waste material will be loaded into a mine car on the surface and dumped at a waste dump near the shaft collar. The GRM has a number

of open stopes underground which will be utilized as a storage space for waste rock to minimize the amount of waste rock stored on the surface.

Ore material will be directly fed from the bin into the crusher of the physical separation facility. Ore will be processed on site by crushing, grinding, and concentration via shaking tables. Tailings will be thickened prior to discharge into a tailings pond. To reduce water usage, water will be reclaimed from the process at the thickener and pumped back into a process water pond. No chemicals, other than Division approved flocculants, will be used in the processing of the ore.

The GRM is designed to operate and close without any discharge or release from the fluid management system except for meteorological events that exceed the design storm limit. The Production Shaft/Headframe Area, Crushing/Grinding Circuit Area, Shop/Process Area, Tailings Impoundment, Process Water Storage Pond, and Waste Rock Dump (collectively referred to as the “Process Containment Area”) are all within 60-mil high-density polyethylene (HDPE) trapezoidal-shaped containment (nominally 150 feet by 130 feet), bermed and graded to drain into a large collection sump.

B. Synopsis

Background: The Antelope District was first organized in 1866 and extends from Poker Brown Gap on the south to Willow Spring area on the north, and from Rye Patch Reservoir to the west flank of the range. Principle mineral commodities found in the district include silver, lead, copper, tin, gold, and zinc with minor amounts of mercury, tungsten, molybdenum, arsenic, antimony, and uranium.

Geology and Mineralogy: The District is characterized by a thick section of argillite, limestone, and quartzite of Triassic age. The Triassic section is intruded by granitic stocks and plugs of late Mesozoic age, by rhyolitic rocks of Tertiary age and by sills and dikes of andesite, dacite, latite, and diorite of pre-Tertiary age. The sedimentary rocks also are cut by veins of quartz, most of which are barren and concordant with the bedding. Majuba Hill, a conspicuous peak in the Antelope Range, is a complex plug about 5,000 feet in diameter that is composed of intrusive rhyolitic rocks and many diverse types of intrusive breccias. Repeated igneous intrusion and explosive activity have produced a very complex sequence of rocks. Irregular dikes of rhyolite porphyry extend for several thousand feet into the sedimentary rocks that surround the plug.

The plug intrudes sedimentary rocks of Triassic age, which consist chiefly of argillite with smaller amounts of quartzite and impure limestone. Intrusive apophyses (e.g., branches or dikes) extend into the metasediment argillaceous rock. The rhyolitic rocks are of three varieties referred to as earlier rhyolite, rhyolite porphyry, and later rhyolite. Five main varieties of intrusive breccia occur in dikes and irregular masses cutting the older rhyolitic rocks. The rhyolitic rocks of the plug and the intruded sedimentary rocks have been silicified, sericitized, and tourmalinized.

Mineralization is hosted in quartz replacement veins that intrude and infill northeast trending shear zones in the metasedimentary rocks and dip from 45° to 70°. The host rock in the area is part of the Auld Lang Syne Group (early Jurassic) composed slate and phyllite. Quartz mineralization underground has been located on the footwall of the shear

zone in thickness of one to two feet. Mineralization in the vicinity of the Gold Ribbon Mine is reported to be a mixture of yellow gold and electrum intergrowths in quartz. Alunite was sometimes present associated with the electrum and fine-grained quartz.

Material Characterization: A meteoric water mobility procedure-Profile I (MWMP-Profile I) characterization results for the ore material showed concentrations of arsenic (0.53 mg/L), nitrate + nitrite (29 mg/L), and TDS (1100 mg/L) all exceeding their respective Profile I reference values. MWMP-Profile I characterization results for the waste rock showed concentrations of arsenic (0.05 mg/L), exceeding its respective Profile I reference value. All ore and waste rock brought to the surface will therefore require placement on lined containment.

Dewatering: The underground workings at the GRM are believed to have been last mined in the early 1960s. The historic workings are currently flooded to approximately 80 feet below the shaft collar. The shaft collar is at an elevation of 5,826 feet above mean sea level (AMSL).

Dewatering water will be pumped to the surface utilizing positive displacement diaphragm pumps powered by compressed air. The suction line for the pump will be below the water level to prevent the pumping of any oils and grease that may have accumulated on the water surface. When the workings have been dewatered, a sump will be constructed to store any infiltration and drill water where the same pumps will pump to the process water pond. In this sump, again the suction line will be below the water line to not pump any oils and grease on the water surface from mine operations. Oil absorbent booms will float on the sump water surface to collect oils and grease and will be disposed of at an approved facility as necessary.

Water will be stored in the Process Water Storage Pond and used for ore processing (e.g., the gravity separation process) on the surface and underground for drill water. There will be a small holding tank (approximately 500 gallons) above the mine site to provide head pressure for process area and underground distribution. Water will be recycled to minimize usage. No additional make-up water will be used on site. If there is additional water volume beyond the holding capacity of the process water pond, alternative management methods will need to be investigated. The quantity of water in the historic mine workings is difficult to quantify since the vertical extent of workings is unknown due to flooding.

Mining: The Permittee plans to extract gold and silver ore from the underground workings by various underground mining methods. Ore will be hoisted out of the production shaft by a skip which will dump into a bin over the primary crusher. Waste rock from underground will be backfilled underground preferentially and if it cannot be backfilled underground, will be hoisted to surface. Once on the surface, it will be dumped from the skip into a mine car and transported to the edge of the waste rock dump for disposal. Any topsoil moved during construction of mining or processing facilities will be stockpiled for use during reclamation.

Waste Rock Dump: As stated previously, the entire Process Containment Area is on 60-mil high-density polyethylene (HDPE) trapezoidal-shaped containment (nominally 150 feet by 130 feet), bermed and graded to drain into a 60-mil HDPE-lined collection sump.

The liner is placed on a compacted soil layer and keyed into a 2-foot wide by 2-foot deep key-in trench.

Nearly all of the waste rock mined will be used as underground backfill, only a small portion will need to be brought to the surface for final disposal and embankment construction. The Waste Rock Dump occupies a trapezoidal-shaped footprint of approximately 1,400 square feet with an estimated capacity of 2,200 tons, based on the maximum height of 15 feet.

Ore Processing and Stockpile: Ore is fed into the primary crusher from a bin under the production shaft headframe. The ore will be crushed by the 8-inch x 10-inch jaw crusher to minus ½-inch. From the jaw crusher discharge, ore will be conveyed to a surge bin for the impact mill, where it will be finely ground to minus 30-mesh for concentration. Ore will be classified to the desired size and any oversize will be re-ground until it is appropriately sized. The material will pass through a magnetic separator to remove any tramp metal from crushing and grinding.

Following magnetic separation, the ore will be discharged to shaking tables for gravity concentration. Make-up water for the gravity process will be pumped from the Process Water Storage Pond and combined with recycled water from the gravity process.

Concentrates will be collected and securely stored for future doré production. Tailings from the shaking tables will go into an 8-foot diameter thickener for dewatering and thickening. Clarified water from the thickener will be further clarified in an 8-foot diameter polishing clarifier and will then return to the process water pond. Thickener underflow will be pumped to the Tailings Impoundment.

Process Water Storage Pond and Tailings Impoundment: The trapezoidal-shaped HDPE-lined Process Water Storage Pond is nominally 90-feet by 28-feet by 10-feet deep with a capacity of 117,000 gallons at two feet of freeboard. A 4-strand wire fence to exclude wildlife and human entry will be installed around the perimeter of the pond. Dewatering water from the underground workings will be pumped to the pond for use in the gravity separation process.

The HDPE-lined Tailings Impoundment is adjacent to the Process Water Storage Pond and occupies a footprint of approximately 5,400 square feet. Approximate capacity at four feet of freeboard is 1,200 tons. Gravity Circuit tailings discharge into an 8-foot diameter thickener for dewatering and thickening. Clarified water from the thickener will be further clarified in an 8-foot diameter polishing clarifier and will then discharge to the Process Water Storage Pond. Thickener underflow will be pumped to the Tailings Impoundment. At the deepest point of the impoundment, a decant tower will be constructed to collect any decanted water. Water from the decant tower will be pumped as necessary to the clarifier.

The Tailings Impoundment will be gently sloped from the upgradient side to allow for equipment to muck out the tailings as necessary for backfill material. A 12-inch layer of tailings will be placed on top of the HDPE liner to serve as a protective layer. Orange snow fencing material placed flat on top of the protective layer will serve as “early warning” to indicate the protective layer has been reached during mucking operations and all mucking must stop. The tailings pond will have a 4-strand wire fence to exclude wildlife and human

entry, with a gate on the side which equipment will enter and exit when mucking out the tailings. Personal flotation devices will be stored at all ponds.

Stormwater Management: As stated previously, run-off from the HDPE-lined Process Containment Area will be collected in a 60-mil HDPE-lined collection sump, nominally 15 feet by 15 feet by 4 feet deep. Any run-off collected is returned back to the Process Water Storage Pond.

An unlined stormwater diversion ditch, approximately 350 feet in length, will be excavated along the north, east and south flanks of the Process Containment Area. The 100 year/24 hour storm event for the Imlay weather station is 2.30 inches. Given the site area below the stormwater diversion ditch of 31,849 square feet, this gives a stormwater volume of approximately 45,000 gallons $((31,849 \times (2.30/12)) \times 7.48)$. Maximum tailings freeboard will be 4 feet from the crest of the tailings dam which will allow 2 feet of freeboard for stormwater collection with 2 feet of total freeboard to the crest at ultimate capacity.

Petroleum Storage: Gasoline, diesel fuel, lubricants, and drilling aids will need to be stored on site. Quantities will be kept to a minimum to reduce the potential of spills and all fuel and bulk lubricants will be stored on containments having at least 110 percent of the volume of the largest container or be double-walled. Any flammables in small containers will be stored in a flammable cabinet. Any Petroleum Contaminated Soils (PCS) will be gathered up and stored in a bin and disposed of off-site at an approved disposal facility as necessary.

C. **Receiving Water Characteristics**

The hydrology of the site is difficult to characterize with the current development. The best estimate is the water level that has flooded the historic mine workings. The true groundwater level may be below the mine workings, and the flooded water may simply be meteoric in nature. Infiltration flows after the mine is dewatered will help with the understanding of the site hydrology.

The historic workings of the Gold Ribbon Mine are currently flooded to approximately 100' below the shaft collar (measured on the incline, approximately 75' vertically). The shaft collar is at an elevation of 5,826 ft. AMSL.

The best estimate of the groundwater gradient is that it flows to an alluvial fan to the northwest of the site below the Antelope Range.

There are no known surface waters within a ½ mile radius. There are a number of unnamed springs and creeks in the draws below the site that are primarily dry. The nearest named water source is Moonshine Spring which is located approximately 1.5 miles west of the site. The town site of Scossa is a ghost town that is located approximately 3.5 miles west of the site. There are no known habitable buildings present within a ½ mile radius. There are no documented drinking water wells within a ½ mile radius, and there are no records of any water wells drilled within Township 33 North, Range 31 East, pursuant to Nevada Division of Water Resources.

Water characterization results obtained from the flooded workings indicate that arsenic (0.47 mg/L), iron (1.8 mg/L), and total dissolved solids (1,800 mg/L) concentrations all

exceed their respective Division Profile I reference values of 0.01 mg/L, 0.6 mg/L, and 1,000 mg/L.

D. Procedures for Public Comment

The Notice of the Division's intent to issue a Permit authorizing the facility to construct, operate and close, subject to the conditions within the Permit, is being published on the Division website: <https://ndep.nv.gov/posts/category/land>. The Notice is being mailed to interested persons on the Bureau of Mining Regulation and Reclamation mailing list. Anyone wishing to comment on the proposed Permit can do so in writing within a period of 30 days following the date the public notice is posted to the Division website. The comment period can be extended at the discretion of the Administrator. All written comments received during the comment period will be retained and considered in the final determination.

A public hearing on the proposed determination can be requested by the applicant, any affected State or intrastate agency, or any interested agency, person or group of persons. The request must be filed within the comment period and must indicate the interest of the person filing the request and the reasons why a hearing is warranted.

Any public hearing determined by the Administrator to be held must be conducted in the geographical area of the proposed discharge or any other area the Administrator determines to be appropriate. All public hearings must be conducted in accordance with NAC 445A.403 through NAC 445A.406.

E. Proposed Determination

The Division has made the tentative determination to issue the renewed Permit.

F. Proposed Effluent Limitations, Schedule of Compliance, Special Conditions

See Section I of the Permit.

G. Rationale for Permit Requirements

The facility is located in an area where annual evaporation is greater than annual precipitation. Therefore, it must operate under a standard of performance which authorizes no discharge(s) except for those accumulations resulting from a storm event beyond that required by design for containment.

The primary method for identification of escaping process solution will be placed on required routine monitoring of make-up water and collection ponds. Specific monitoring requirements can be found in the Water Pollution Control Permit.

H. Federal Migratory Bird Treaty Act

Under the Federal Migratory Bird Treaty Act, 16 U.S. Code 701-718, it is unlawful to kill migratory birds without license or permit, and no permits are issued to take migratory birds using toxic ponds. The Federal list of migratory birds (50 Code of Federal Regulations 10, 15 April 1985) includes nearly every bird species found in the State of Nevada. The U.S. Fish and Wildlife Service (the Service) is authorized to enforce the prevention of migratory bird mortalities at ponds and tailings impoundments. Compliance with State permits may

not be adequate to ensure protection of migratory birds for compliance with provisions of Federal statutes to protect wildlife.

Open waters attract migratory waterfowl and other avian species. High mortality rates of birds have resulted from contact with toxic ponds at operations utilizing toxic substances. The Service is aware of two approaches that are available to prevent migratory bird mortality: 1) physical isolation of toxic water bodies through barriers (e.g., by covering with netting), and 2) chemical detoxification. These approaches may be facilitated by minimizing the extent of the toxic water. Methods which attempt to make uncovered ponds unattractive to wildlife are not always effective. Contact the U.S. Fish and Wildlife Service at 1340 Financial Boulevard, Suite 234, Reno, Nevada 89502-7147, (775) 861-6300, for additional information.

Prepared by:

Date:

Fact Sheet Revision 00

Keith Johnson

September 24, 2026

Renewal 2026, Boilerplate Update