FACT SHEET
(Pursuant to Nevada Administrative Code (NAC) 445A.401)

Permittee Name: **Barrick Turquoise Ridge, Inc.**

Project Name: **Getchell Mine Project**

Permit Number: **NEV0086014**
Review Type/Year/Revision: **Renewal 2016, Fact Sheet Revision 00**

A. Location and General Description

Location: The Barrick Turquoise Ridge, Inc. (BTRI**)** Getchell Mine Project is located in Humboldt County, approximately 30 miles northeast of Winnemucca, Nevada. The project is accessed by traveling 15 miles east of Winnemucca on U.S. Interstate-80 to the Golconda exit, then traveling approximately 25 miles north on State Route-18 (Getchell Mine Road) to the mine site. The mine facilities are located on both public land administered by the Bureau of Land Management Humboldt River Field Office, and private land in Sections 1-5, 7-23, 25-29, and 32-36, Township 39 North (T39N), Range 42 East (R42E); Sections 1-6, 9-15, and 17, T38N, R42E; and Sections 5, 6, 8, 15, and 16, T38N, R43E, Mount Diablo Baseline and Meridian (MDB&M).

General Description: The permitted mining facilities consist of several inactive open pit mines, the Turquoise Ridge Underground (TRU) and the inactive Getchell Main Underground (GMU) mines, headframes, limestone and basalt quarries, waste rock dumps, ore stockpiles, offices, shops and ancillary support facilities. Processing and support service facilities include administrative offices, tailings impoundment, heap leach facility (in closure), maintenance shops, fuel depots, storage areas, and a security/warehouse complex. Ancillary facilities include batch plants for underground backfill, water supply and dewatering wells, service water system, truck wash, pipelines, powerlines, topsoil stockpiles, Class III waivered landfill, and reclamation test plots. The facility is required to be designed, constructed, operated and closed without any discharge or release in excess of those standards established in regulation except for meteorological events which exceed the design storm event. Ore production is limited by the Permit to 2,000,000 tons per year for shipment to an off-site processing facility.

B. Synopsis

General: BTRI, a wholly owned subsidiary of Barrick Gold Corporation, is the current Permittee of the mine, which has been intermittently operated since 1937. Gold production began in 1938, and continued through World War II. Processing through the mill of tungsten ores mined from the Riley Mine, adjacent to the

Getchell Mine, occurred from 1951 to 1959. Gold production resumed from 1961 to 1969 from four open pits and from underground workings.

Conoco received permission from the Division in 1982 to re-leach some of the historic tailings for gold recovery. However, the operation was never initiated and the property was sold to FRM Minerals, a subsidiary of the First Mississippi Corporation, in 1983. FRM Minerals became Getchell Gold Corporation (GGC) in 1996 through corporate succession. GGC was purchased by Placer Dome America in 1999, which merged with Barrick Gold Corporation in 2006. The mine continues to be operated by BTRI.

Underground mining of sulfide ores resumed in 1994 from adits in the Getchell Main Pit (the GMU mine). The Turquoise Ridge ore body was discovered in 1995 and is currently accessed by two shafts (the TRU mine). Due to the drop in gold prices, TRU and GMU ore production ceased in 1999 and 2000, respectively. All milling and processing operations at the mine were suspended in late 1999. In December 2002, the GMU operation was restarted, and by April 2003, the restart plan for the TRU was finalized and initiated. In September of that year, a joint venture was formed between Placer Turquoise Ridge, Inc. (PTRI) and Newmont Mining Corporation to include the sale of ore to Newmont's neighboring Twin Creeks operation. As such, the beneficiation facilities at the mine were not required to be brought back into operation at that time. Currently, all ore from Getchell is shipped off-site for processing at Newmont's Twin Creeks operation. The Permittee anticipates that the mine has at least 20 years of operation remaining, based on present ore reserves. In 2006, PTRI changed its name to BTRI to reflect ownership by Barrick.

Open Pits: Historical operations lead to the development of eight open pit mines at the site. The North, Center, South, and Hansen Creek pits were developed during the 1930's to 1960's. The Center and South pits were later combined to create the Getchell Main Pit, and extended into the North Pit. Previous operators also extended the Hansen Creek Pit, and developed the North Hansen Creek and Summer Camp pits (farther south along the Getchell Fault), and the newer Turquoise Ridge and Valmy pits (along a small ridge southwest of the old mill site). With the exception of the Hansen Creek Pit and the southern portion of the Getchell Main Pit, the pits are located on private land owned by the Permittee.

Currently, all ore production is from the TRU. Mining in the GRU was suspended in 2008, and the infrastructure was removed from the underground workings. Mining in the open pits ceased for sulfide ores in 1995, and for oxide ores in 1996; however, some ore reserves remain at the Hansen Creek and Getchell Main pits. These reserves may be mined in the future, pending economic considerations. Waste rock from the pits would be placed on existing dumps and

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within existing dump footprints, or would be placed as backfill into existing pits located on private ground.

In addition to the gold ore bodies, the mine developed a small limestone quarry on private land in Section 21 (T39N, R42E) and on public land in Section 22 (T39N, R42E) MDB&M, to supply limestone for the milling operation (now inactive), and for backfilling of the Summer Camp Pit. Additionally, limestone is mined for backfill production for use at TRU. Associated with this limestone quarry are stockpiles, a waste rock dump, and an access road. A small basalt aggregate quarry (Bud Hill) near Turquoise Ridge was developed in 1998 to supply aggregate for cement backfill used in the underground operations.

Final closure of the mine is predicted to leave a surface water body in the Getchell Main Pit when groundwater has recovered after cessation of dewatering. As this pit will be a permanent surface feature, the chemical composition of the predicted lake is an important aspect in the evaluation of potential environmental impacts in the long term. The North Pit is predicted to remain dry except for seasonal accumulations of meteoric water.

Pit lake studies predict that the Getchell Main Pit will be an evaporative sink, resulting in no significant outflow to adjacent groundwater. The quality of the pit water after 100 years is predicted to have a circum-neutral pH (7.9 S.U.) and to meet Profile I reference values except for TDS (1,500 milligrams/liter [mg/L]), sulfate (950 mg/L), arsenic (0.8 mg/L), antimony (0.045 mg/L), nickel (0.24 mg/L), and thallium (0.004 mg/L). A Screening Level Ecological Risk Assessment (SLERA) conducted using the results of the pit lake water quality study showed no significant hazard to human, terrestrial, or avian life.

The Hansen Pit, North Hansen Pit, waste rock dump, and adjacent Hansen Creek disturbances were reclaimed during 2004. This included limestone backfilling within pit depressions, uniform limestone placement on exposed sulfide surfaces, pit highwall regrading, topsoil placement, and seeding. The North Hansen Pit was regraded to be free-draining so that no surface water would accumulate. The small pit lake in the Summer Camp Pit has been mitigated through removal of sediments discharged from the underground operations during the 1990's and backfilling above the predicted steady-state water table elevation with limestone from the quarry.

Underground Mines: In 1994, the Permittee began development of the deep ore bodies through four adits and extensive underground workings accessed from the Getchell Main Pit. In 1996, underground development of the new Turquoise Ridge ore body began. Mining of the GMU was suspended in 2008.

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Work is ongoing at the TRU including, exploration, underground development, and mining. At the TRU all ore and waste materials are hoisted to the surface through a single shaft and placed in temporary stockpiles according to mineral grade.

A minor modification was completed in March 2015 for the addition of the Shaft #3 complex which will be located 1 mile northeast of the existing shaft #1. The new shaft is required to improve underground ventilation, shorten the distance from the underground working areas, and increase hoisting capacity. The facility consists of a new 24-foot diameter shaft with associated collar, head-frame, ancillary support, and ore handling facilities. The project will require a temporary ore storage facility adjacent to the shaft and an expansion of the existing ore stockpile located immediately upgradient and west of the old mill site. The increased hoisting capacity with the addition of Shaft #3 will not exceed the project overall Permit limit of 2,000,000 tons of ore per year. Storage vessels or tanks used to store backfill additives, shotcrete accelerator, and emulsion will be located within concrete containment structures designed to handle 110 percent of the volume of the largest tank. The site includes 2 unlined stormwater retention basins and a double-lined and leak detected stormwater runoff pond for the ore and waste rock temporary storage area. The retention basins are designed to collect and contain runoff from a 100-year, 24-hour storm event plus 2-foot of freeboard for the west retention basin and 0.8-foot of freeboard for the East Retention Basin. The stormwater system diverts non-contact water around the mine facilities and discharges to downstream water courses; conveys sediment laden runoff to detention basins before being discharged to downstream water courses; and contains precipitation that has come in contact with ore or process components.

Ore Stockpiles: Three ore stockpile areas have been designed and built to preclude degradation of the waters of the State. These stockpiles include the low-grade ore and reactive waste stockpile west of the administrative building; the ore stockpile immediately upgradient and west of the old mill site, and the radial stacker ore stockpile adjacent to the Turquoise Ridge shaft complex. As a part of the March 2015 minor modification, the stockpile west of the old mill site will be upgraded and an additional temporary stockpile will be constructed at the Shaft #3 complex.

The low-grade ore and reactive waste stockpile was completed in April 2004. The stockpile base consists of a 12-inch soil layer compacted to a minimum of 92% of maximum dry density, to achieve a maximum permeability of $1x10^{-5}$ cm/s. The base of the stockpile is graded to the east where a 60-mil high density polyethylene (HDPE)-lined drainage ditch collects and conveys runoff to a concrete sump. The sump measures 10½ feet by 8 feet and includes an 18-inch high overflow weir to promote settling of fines prior to discharge of accumulated

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runoff. The sump walls are 4-inch thick concrete with waterstops at each joint. The discharge point consists of an 8-inch diameter HDPE pipe which conveys collected runoff east to the tailings pipeline which discharges into the tailings impoundment.

The ore stockpile west of the old mill site was completed in June 2003. The stockpile base consists of a 12-inch soil layer compacted to a minimum of 90% of maximum dry density to achieve a maximum permeability of $1x10^{-5}$ centimeters/second (cm/s). The soil layer is covered with a 24-inch thick drainage layer which is comprised of drain rock and a network of 4-inch diameter perforated chlorinated polyethylene (CPE) pipe. The base of the stockpile is graded to the east where a HDPE-lined drainage ditch collects and conveys runoff to three concrete sumps. Each sump measures 6½ feet by 4 feet and includes an 18-inch high overflow weir to promote settling of fines prior to discharge of accumulated runoff. The sump walls are 4-inch thick concrete with water stops at each joint. The discharge from each sump consists of a 6-inch diameter HDPE pipe which conveys collected runoff east to the tailings pipeline which discharges into the tailings impoundment.

The existing facility is approximately 350,000 square feet, oriented in a north south direction with measurements of 1,400 feet by 250 feet. The increase in production from the installation from Shaft #3 will require an expansion of this stockpile. The current facility is sized to contain 180,000 tons at an average stack height of 25 feet. The expansion will increase the storage to 230,000 tons by adding 100,000 square feet to the southeast. The stockpile base consists of a 12-inch soil layer compacted to a minimum of 92% of maximum dry density to achieve a maximum permeability of $1x10^{-5}$ cm/s. The soil layer will be covered with a 24-inch thick drainage layer which is comprised of drain rock and a network of 4-inch diameter perforated CPE pipe. The base of the expanded stockpile area is graded to the east where a HDPE-lined drainage ditch collects and conveys runoff to the central low point (sump). This sump will replace the existing 3 sumps and collect runoff from both the existing stockpile and expansion area. At the sump, there will be a 36-inch diameter HDPE pipe that will serve as a drop inlet with a low level outlet pipe (12-inch diameter HDPE pipe). The outlet pipe will tie to the existing mill tank that is equipped with outlet pipes that drain into the tailings impoundment.

Dewatering for the new Shaft #3 will require the installation of 2 new dewatering wells which are permitted under the Getchell Infiltration Project Discharge Permit NEV0095113.

The Shaft #1 radial stacker ore stockpile was completed in January 2005. The stockpile base consists of a 6-inch soil layer compacted to a minimum of 92% of maximum dry density to achieve a maximum permeability of $1x10^{-5}$ cm/s. The

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base of the stockpile is graded to the north where a compacted soil-lined drainage ditch collects and conveys runoff to a concrete sump. The sump measures 9.5 feet by 8 feet and includes an 18-inch high overflow weir to promote settling of fines prior to discharge. The design also includes a 3 horizontal:1 vertical (H:V) sloped ramp to allow access for a small loader to remove accumulated sediments. The sump walls are 6-inch thick concrete with water stops at each joint. The discharge from the sump consists of a 6-inch diameter HDPE pipe which conveys collected runoff east to the 16-inch diameter emergency pipeline.

The Shaft #3 ore and waste will be transported to the belt offload stockpile load out pad. The pad is designed to contain 2 days' worth of ore and waste combined or three days' worth of ore production only. The containment area is 550 feet by 350 feet and accommodates the 125-foot radial stacker, ore and waste stock piles, evaporation storm pond, and room to maneuver mining equipment. The pad consists of a 1 foot thick layer of low permeability soil compacted to a minimum of 92% of maximum dry density to achieve a maximum permeability of $1x10^{-5}$ cm/s, overlain by 2 feet thick drainage layer which is comprised of drain rock and a network of 4-inch diameter perforated (CPE) pipe. The pad slopes at approximately 2.5% to the southwest edge of the pad. Stormwater runoff will drain to the runoff collection evaporation pond which is double-lined with 80-mil HDPE textured geomembrane with an intermediate geonet drainage layer. The approximate pond dimensions are 224 feet long by 50 feet wide and 8 feet deep. The pond has a leak collection and recovery system (LCRS) that will be monitored using a leak detection port. The pond is designed to collect and contain runoff from a 100-year, 24-hour storm event plus 2 feet of free board. If pond levels are not sufficiently managed through evaporation, the water will be pumped into a truck and transported to an approved disposal location.

The Main Waste Rock Dump also contains a low-grade ore stockpile. This low-grade ore was regraded, capped with 18 inches of basalt followed by placement of growth media, and reseeded during the summer of 2004. Even though this material has been covered and reclaimed, it could still have some economic viability and may be removed and processed in the future.

Waste Rock Dumps: Waste rock disposal facilities (dumps) at the site consist of 7 primary waste rock dumps located near the various open pits on both private and public land. All waste that has a potential to degrade waters of the State will be managed in accordance with the "Waste Rock Management Plan" (WRMP), 28 April 2006, included in the application.

Materials characterization was completed for the Shaft #3 installation and it has been determined that the rock wastes generated from the production shaft construction can be managed adequately via the current waste rock management plan which calls for no segregation of reactive waste rock or other special

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handling, isolation practices, or reclamation practices other than those already described in the WRMP. There is sufficient overall acid neutralizing capacity to inhibit acid rock generation by infiltration through mixed waste.

Bioremediation Facility: In the past, the Permittee operated a lined bioremediation facility for the treatment of hydrocarbon-impacted soil and sediment. The facility is located on an inactive portion of the main waste rock dump, and was designed, constructed and is operated under the requirements of General Permit #HGP-24. In June 2009, the Permittee submitted an engineer design change (EDC) to incorporate a Petroleum Contaminated Soil (PCS) Management Plan into the Permit. The EDC was approved by the Division in February 2013, thereby superseding the general permit.

Onsite Water System: Two systems provide the mine with water for consumptive use and for use around the mine. The potable water system consists of one well, WW-4, that is located south of the Twin Creeks mine. The mine service water system pumps treated water from the tail end of the water treatment plant (WTP). The WTP water is used for haul road dust suppression, construction, reclamation, and underground mine service.

Mill Facility: Mill processing was suspended in late 1999, and all mill facilities have been removed. A detailed description of the mill facilities, as they existed when active, is provided in the Permit application. The thickener remains, but was drained and recommissioned under a modification to the Care and Maintenance Plan, to allow the Permittee to manage the petroleum hydrocarbon-impacted sediments from the mine dewatering and treatment system, as necessary. Since suspension of mill operations, all ore produced has been shipped off-site for processing.

Historic Tailings Impoundment: Beginning in 1938, and up to 1983, tailings were deposited in an uncontained area located to the east of the old mill site, in Sections 33, 34, and 35. FRM voluntarily began reclaiming the historic tailings in 1991, in consultation with the Bureau of Land Management (BLM) and the Division. The historic ('old') tailings impoundment was capped in 1996, with a 2-foot to 10-foot layer of inert waste rock and growth media, followed by revegetation. Several monitoring wells are present in the vicinity of the old tailings, which indicate improving groundwater quality with the exception of total dissolved solids (TDS) and arsenic. Although the majority of the historic tailings have been capped with waste rock, some areas remain uncovered. The Permittee has covered all of the significant areas of historic tailings in Section 34 with approximately 2-feet of waste rock in accordance with a BLM 3809 Plan Amendment. Smaller areas of tailings in Section 35 and 36 have a thin layer (up to a few inches) of tailings material which was deposited during an embankment washout in the 1960s. These areas will be inspected to ensure that the tailings are

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sufficiently thin to allow vegetative growth, in which case the areas will remain as they are without additional reclamation.

Current Tailings Impoundment: The first stage of the impoundment, constructed in 1989, consists of an embankment of earth and screened rock that fills a valley between two bedrock hills, and was designed as a synthetically-lined, zero-discharge facility. The embankment has internal chimney drains that route process water to the underdrain system located above the liner. Fluid in the underdrain system reports to a dedicated sump located near the outside toe of the embankment, from where it is pumped back to the impoundment.

Since the tailings facility was first constructed, the embankment has been raised 4 times (Stages 2 through 5) to the current crest elevation of approximately 5,128 feet above mean sea level (amsl). During past milling operations, tailings from the CIL tanks were pumped as slurry to the tailings impoundment. The tailings were deposited using managed, sub-aerial techniques (perimeter spigotting) that maximized evaporation of solution and consolidation of the tailings solids, minimized the supernatant pond area, and kept the pond away from the dam face.

The impoundment is designed to accommodate direct precipitation and run-on from minor watershed areas to the north and east resulting from the 100-year, 24-hour, storm event. A diversion structure, designed to redirect peak flows from a 100-year, 24-hour storm event, was constructed around the west side of the impoundment to prevent erosion of the embankment by runoff from the upgradient watershed.

Heap Leach Pad Facilities: Closure of the Getchell heap leach pad facilities was initiated in 2001. As part of the closure program, a soil cover was placed over the heaps and the off-loaded material, and an evaporation pond system was designed and constructed using existing process ponds to dispose of the long-term heap drainage solutions. These systems are believed to provide adequate protection against degradation of waters of the State. If necessary, excess water in the evaporation ponds is hauled to the tailings impoundment using water trucks. A monitoring program has been designed to validate the performance of the closure systems. In addition, an infiltration field was designed (but not yet constructed) adjacent to the pad and evaporation ponds that will receive overflow from the system in the event that the evaporative capacity of the ponds is exceeded during extreme storm events once work crews are no longer present on site to manage draindown.

Stormwater Ditches and Controls: The Permittee has constructed a system of stormwater diversion ditches to protect the facilities from damage resulting from the 100-year, 24-hour storm event, and reduce soil and sediment migration. All

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diversion ditches and stormwater controls will be maintained during the life of the mine and during closure.

Petroleum-Contaminated Soil (PCS) Management Plan: A PCS Management Plan was approved as an EDC in February 2013, authorizing on-site disposal of PCS on the Main Waste Rock Dump near the old Bioremediation Facility (site DL-1 – primary), and on the closed heap leach pad (site DL-2 – secondary). Prior to management under the plan, hazardous waste determinations must be performed to demonstrate that the PCS is not hazardous waste. Hazardous waste must be managed and disposed of in accordance with applicable regulations. On-site disposal of PCS is also contingent on the results of periodic screening analyses, which must show that the PCS does not exceed screening levels for various organic constituents established via risk assessment. Otherwise, the PCS must be properly disposed of off-site. PCS may be stored on temporary holding pads (former bioremediation pads) while screening analyses are performed, or it may be provisionally placed at one of the approved disposal locations provided that it will be removed and properly disposed of elsewhere if it exceeds screening levels during subsequent screening analyses. Various time limits and other stipulations in the plan apply to temporary storage and provisional placement of the PCS.

C. Mine Site Hydrology & Hydrogeology

Surface Water: The Getchell Mine is located within the Great Basin hydrologic region, which is characterized by an internal drainage system where runoff collects in the valley basins and eventually evaporates. The source of water in the region is predominantly from precipitation at higher elevations (predominantly snowmelt) to the west of the mine that feeds small drainages such as Summer Camp and Hansen Creeks. Once these creeks exit the mountain source areas, the water infiltrates the alluvial ground surface, recharging groundwater resources. Although these drainages connect to Kelly Creek Valley, the streams are ephemeral, only flowing to Kelly Creek following significant storm events.

Two other creeks upgradient of the property, Granite Creek and Rocky Canyon Creek have been permanently diverted into the North Hansen Creek Pit. This water is used as mine service water or sent to the Water Treatment Plant (WTP). The WTP and associated facilities are permitted under WPCP NEV95113.

There are 2 unnamed drainages in the valley downgradient of the tailings impoundment area. The confluence of these drainages runs along the base of the left abutment downstream of the impoundment and flows to the southeast into Kelly Creek. The drainages are dry and flow only for short periods following infrequent heavy storms.

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Groundwater: The Permittee primarily utilizes fresh water from water supply well WW-4, with well WW-1 used as a back-up, both of which are located about four miles southeast of the mine site. The wells were installed in 2011 and 1948, respectively. Production well WW-2 was abandoned in 2007. Wells WW-1 and WW-4 produce water from alluvial aquifers located in the Kelly Creek Basin. Currently, well WW-1 exceeds the Profile I reference value for arsenic, and may require treatment if used in the future; arsenic concentrations in WW-4 are below the Profile I reference value. Two additional water supply wells, HL-1 and HL-2, are located adjacent to the heap leach facility (in closure), but are no longer used as production wells.

Since 2006, 7 monitoring wells have dried up and have, therefore, been abandoned and replaced. These include TIMW-2 (replaced by TIMW-2A), TIMW-4 (replaced by TIMW-4A), TIMW-6 (replaced by TIMW-6A), MMW-1 (replaced by MMW-1A), MW-9 (replaced by MW-9A), MW-10 (replaced by MW-10A), MW-11 (replaced by MW-11A), and MW-12 (replaced by MW-12A). In addition, monitoring well TIMW-12 was added in 2011, and wells NZMW-01, NZMW-02, and NZMW-03 were proposed as part of the Permit renewal of 2011, to be added downgradient of the North Zone Backfill area. The addition of these wells was approved by the Division in November 2011.

Numerous groundwater studies have concluded that groundwater production in the area of the mine varies depending on the geologic unit in which the wells are installed. Unaltered and fractured bedrock and some portions of the ore zones, produce the largest volumes of groundwater, while clay-altered rocks and the granodiorite on the west side of the Getchell fault zone produce limited amounts of groundwater. Regional groundwater in the vicinity of the closed heap leach facility is hosted entirely by alluvial materials to a depth of at least 450 feet below the ground surface (bgs). The static water level in heap leach water supply well HL-1, during drilling in 1986, was at 264 feet bgs. During a pump test in 1992, the static water level was as 256 feet bgs, while sampling in 1997 indicated static water levels of approximately 249 feet bgs. Groundwater flow is easterly, toward the Kelly Creek Basin.

Condemnation holes drilled in the area of the tailings impoundment indicate a water level between 105 and 335 feet bgs, and typically more than 200 feet bgs. The Permittee has installed 8 monitoring wells around the perimeter of the impoundment which are monitored quarterly.

Groundwater from the bedrock aquifers in and around the active underground operations at the mine can be classified into three different types based on their background water quality and on their proximity to mineralized zones:

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Type 1: waters from areas away from the sulfide mineralization or from formations containing significant marble that is Ca-HCO_3-dominated.

Type 2: waters from sulfide mineralized zones that are Ca-HCO_3-SO_4-dominated.

Type 3: waters from sulfide mineralized zones that are Ca-Na-SO_4 dominated.

All of these water types are typically alkaline, with Type 1 having a pH range higher than the others. Type 1 waters typically contain a range of the constituents aluminum, arsenic, iron and manganese in excess of Profile I reference values. Type 2 and 3 waters typically contain a range of the constituents including TDS, sulfate, aluminum, arsenic, iron, manganese and zinc in excess of Profile I reference values. Type 2 and 3 waters contain arsenic and iron in a reduced oxidation state as well as dissolved sulfide with other minor elements. Type 2 waters dominate groundwater flowing into the GMU and TRU mines. Operations will continue to encounter this water for the foreseeable future and changes in the quality of this water could require modifications to the mine water handling system (WPCP NV0095113). The quality of the groundwater flowing into the GMU and TRU mines shows a range of water chemistry similar to that observed in the USGS database for the area.

D. Procedures for Public Comment

The Notice of the Division's intent to issue a Permit authorizing the facility to construct, operate, and close, subject to the conditions within the Permit, is being sent to **The Humboldt Sun** for publication. The Notice is being mailed to interested persons on the Bureau of Mining Regulation and Reclamation mailing list. Anyone wishing to comment on the proposed Permit can do so in writing within a period of 30 days following the date of public notice. The comment period can be extended at the discretion of the Administrator. All written comments received during the comment period will be retained and considered in the final determination.

A public hearing on the proposed determination can be requested by the applicant, any affected State, any affected intrastate agency, or any interested agency, person or group of persons. The request must be filed within the comment period and must indicate the interest of the person filing the request and the reasons why a hearing is warranted.

Any public hearing determined by the Administrator to be held must be conducted in the geographical area of the proposed discharge or any other area the Administrator determines to be appropriate. All public hearings must be conducted in accordance with NAC 445A.403 through NAC 445A.406.

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E. Proposed Determination

The Division has made the tentative determination to issue the renewed Permit.

F. Proposed Limitations, Schedule of Compliance, Monitoring, Special Conditions

See Section I of the Permit.

G. Rationale for Permit Requirements

The facility is located in an area where annual evaporation is greater than annual precipitation. Therefore, it must operate under a standard of performance which authorizes no discharges except for those accumulations resulting from a storm event beyond that required by design for containment.

The primary method for identification of escaping process solution will be placed on required routine monitoring of leak detection systems as well as routinely sampling downgradient monitoring wells and surface water. Specific monitoring requirements can be found in the Water Pollution Control Permit.

H. Federal Migratory Bird Treaty Act

Under the Federal Migratory Bird Treaty Act, 16 U.S. Code 701-718, it is unlawful to kill migratory birds without license or permit, and no permits are issued to take migratory birds using toxic ponds. The Federal list of migratory birds (50 Code of Federal Regulations 10, 15 April 1985) includes nearly every bird species found in the State of Nevada. The U.S. Fish and Wildlife Service is authorized to enforce the prevention of migratory bird mortalities at ponds and tailings impoundments. Compliance with State permits may not be adequate to ensure protection of migratory birds for compliance with provisions of Federal statutes to protect wildlife.

Open waters attract migratory waterfowl and other avian species. High mortality rates of birds have resulted from contact with toxic ponds at operations utilizing toxic substances. The Service is aware of two approaches that are available to prevent migratory bird mortality: 1) physical isolation of toxic water bodies through barriers (covering with netting), and 2) chemical detoxification. These approaches may be facilitated by minimizing the extent of the toxic water. Methods which attempt to make uncovered ponds unattractive to wildlife are not always effective. Contact the U.S. Fish and Wildlife Service at 1340 Financial

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Boulevard, Suite 234, Reno, Nevada 89502-7147, (775) 861-6300, for additional information.

Prepared by: Michelle Griffin
Date: Day Month 2016

Revision 00: New Permit.

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