NV Energy

SCI-081
TEMP

April 7, 2016

Ms. Alison Oakley
Nevada Division of Environmental Protection – Bureau of Corrective Actions
901 South Stewart Street
Carson City, NV 89701

**Re: NV Energy**
**Reid Gardner Generating Station Facility ID# H-000530**
**Source Area 8 Groundwater and Soil Characterization Work Plan**

Dear Ms. Oakley,

NV Energy is pleased to submit the final Reid Gardner Source Area 8 Groundwater and Soil Characterization Work Plan for your review.

If there are any questions regarding this submittal, please contact the undersigned at 702-402-5958.

Respectfully Submitted,

Jason Reed
Senior Environmental Adviser
NV Energy

CC: William Campbell, NDEP (electronic copy via FilesAnywhere)
Michael Rojo, NV Energy
Tony Garcia, NV Energy (two copies)
John Kivett, ARCADIS U.S., Inc.
Bob Forsberg, ARCADIS U.S., Inc.

NEVADA DIVISION OF
**ENVIRONMENTAL PROTECTION**

**STATE OF NEVADA**
Department of Conservation & Natural Resources
Brian Sandoval, Governor
Leo M. Drozdoff, P.E., Director
David Emme, Administrator

March 18, 2016

Jason Reed
Senior Environmental Advisor
NV Energy
6226 W Sahara Ave M/S 30
Las Vegas, NV 89146

Re: **NV Energy (NVE)**
**Reid Gardner Station (RGS)**
**NDEP Facility ID #H-000530**
Nevada Division of Environmental Protection Concurrence with: *Source Area 8 Groundwater and Soil Characterization Work Plan, Administrative Order on Consent Activities*, Draft March 2016

Dear Mr. Reed:

The Nevada Division of Environmental Protection (NDEP) has received and reviewed NV Energy's (NVE's) Draft Work Plan for Source Area 8 (SA-8), Units 1, 2, 3 Catch Basin. The work plan is dated March 8, 2016 and was received by the NDEP on March 15, 2016.

The work plan presents site characterization work to delineate potential soil and groundwater impacts at the Units 1, 2, 3 Catch Basin. The Catch Basin was originally constricted to contain storm water runoff and cooling tower overflows. Based on review of the Response to Comments to the February 16, 2016 Draft Work Plan for SA-8 and the changes made to the Work Plan, the NDEP has additional comments to the Draft Work Plan:

1. Page 2-2, Section 2.3, first full paragraph of page:
   Please clarify which version of ProUCL will be used. Will ProUCL be run for all distributions, or a selection of distributions? Please clarify how will non-detects be treated.

2. Page 7-1, Section 7
   Please add the full citation for the version of ProUCL that will be used to evaluate the data.

The NDEP **concurs** with the Work Plan and requests that these clarifications be addressed in the Final version of the Work Plan.

Please contact me with any questions or comments about this letter at (775) 687-9396 or aoakley@ndep.nv.gov

Sincerely,

Alison Oakley, CEM
Environmental Scientist III
Bureau of Corrective Actions

ec: Jeff Collins, Nevada Division of Environmental Protection (NDEP)
Scott Smale, Bureau of Corrective Actions, NDEP Carson City
Todd Croft, Bureau of Corrective Actions, NDEP Las Vegas
Bill Campbell, Tribal Liaison, NDEP
Joe Maez, Bureau of Water Pollution Control, NDEP, jmaez@ndep.nv.gov
Nikita Lingenfelter, Bureau of Water Pollution Control, NDEP, nlingenfelter@ndep.nv.gov
Ebrahim Juma, Clean Water Team (ejuma@cleanwaterteam.com)
Joe Leedy, Clean Water Team (jleedy@cleanwaterteam.com)
Lynn M. Cintron, Southern Nevada Health District, (cintron@snhdmail.org)
Jacqueline Reszetar, Director of Envi. Health, Southern Nevada Health District reszetar@snhdmail.org
Brian Northam, Southern Nevada Health District, (northam@snhdmail.org)
Walter Ross, Environmental Health Supervisor/Engineer (Ross@snhdmail.org)
Andy Chaney, Southern Nevada Health District, (chaney@snhdmail.org)
Donna Houston, Southern Nevada Health District, (houston@snhdmail.org)
Starla Lacy, NV Energy (SLacy@nvenergy.com)
Don Hopper, NV Energy (DHopper@nvenergy.com)
Tony Garcia, NV Energy (TGarcia@nvenergy.com)
Michael Rojo, NV Energy (MRojo@nvenergy.com)
Jason Reed, NV Energy (JReed@nvenergy.com)
Matt Johns, NV Energy (MJohns@nvenergy.com)
Becky Svatos, Stanley Consultants, Inc., (SvatosBecky@stanleygroup.com)
William Carrig, Stanley Consultants, Inc., (CarrigBill@stanleygroup.com)
John Kivett, ARCADIS, (John.Kivett@arcadis.com)
Brad Cross, ARCADIS, (Brad.Cross@arcadis.com)
Ginger Somerville, ARCADIS, (Ginger.Somerville@arcadis.com)
Elliott Lips, Great Basin Earth Science, (elips@gbearthscience.com)
Andrea Issod, Sierra Club, (andrea.issod@sierraclub.org)
Robert Wiygul, Counsel Sierra Club and Moapa Band of Paiutes, (Robert@waltzerlaw.com)
Ranajit Sahu, Consultant, (sahuron@earthlink.com)

cc: Robert Tom, Moapa Band of Paiutes, Chairperson, P.O. Box 340, Moapa, NV 89025
Moapa Band of Paiutes, Environmental Director, P.O. Box 340, Moapa, NV 89025
Clark County Emergency Management, 500 S. Grand Central Parkway 6th Floor, P.O. Box 551713, Las Vegas, NV 89155-1713
Anitha Rednam, Department of Water Resources, 1416 9th Street, Room 1140, Sacramento CA 9581

# Document and Response to Comments Tracking Form
## NV Energy – Reid Gardner Station
## Administrative Order on Consent Implementation

**Document Title** SA-8 Groundwater and Soil Characterization Work Plan

**Preparer** Stanley Consultants, Inc.

---

**Draft #1**

| | | | |
|---|---|---|---|
| To | NDEP | From | NV Energy |
| Submittal Date | 2/16/2016 | Comment Date | 2/22/2016 |
| Response Date | 3/4/2016 | | |
| Commenter | Alison Oakley | Responder | Jason Reed |

Specific Comment #1

*<u>Page 1-1, Section 1.1, 1st sentence (editorial):</u> Please remove the extra period from the end of the sentence.*

Specific Comment #1 Response

The extra period from the end of the sentence was removed.

Specific Comment #2

*<u>Page 2-2, Section 2.3, 1st full paragraph:</u>*
*a. (editorial). Change the second sentence to read "During the first mobilization five soil samples will be collected at depths of 0.0-0.5 feet."*
*b. Table 2-1 on page 2-3 shows the 5 samples (B1-B5), but also has a B-6 with 0.0-0.5 foot sample. Please add an explanation on page 2-2 as to why sample B6 will not be collected at the same time as the other 5 samples.*

Specific Comment #2 Response

a. The report was revised to read "During the first mobilization five soil samples will be collected at depths of 0.0-0.5 feet."
b. The additional sample location (B-6) may be needed in order to conduct a statistical evaluation should there be impacts from the first mobilization. At least 12 total soil samples are needed to conduct a statistical evaluation using the EPA software ProUCL to determine the 95% Upper Confidence Limit (UCL). If the calculated 95% UCL is at or below the BCLs and BTVs, then we can conclude that the area needs no further investigation or cleanup.

Specific Comment #3

*Page 2-2, Section 2.3, 1st full paragraph on page:* *The fourth sentence states "If there is not an EPA RSL, then the analytical results will be compared to the site-specific background threshold values (BTVs) or the NDEP Basic Contaminant levels (BCLs)." Please provide the criteria for determining which standard will be used.*

Specific Comment #3 Response

The results will be first compared to the EPA RSL, if there is no EPA RSL for a specific analytical result then the result will be compared to the site-specific BTVs or BCLs. Page 2-2 was revised to state "If the calculated 95% UCL is at or below the BCLs and BTVs, then the area needs no further investigation or cleanup".

Specific Comment #4

*Pages 2-4, Section 2.3 Note 5 for Table 2-1:* *The comment states "At least 12 total soil samples are needed to conduct a statistical evaluation using the 95% Upper Confidence Limit (UCL). The statistical evaluation will be used to determine whether additional soil excavation is necessary." Please include a discussion of the methodology of the proposed statistical evaluation in the text.*

Specific Comment #4 Response

EPA software ProUCL will be used to determine the 95% UCL. If the calculated 95% UCL is at or below the BCLs and BTVs, then the area needs no further investigation or cleanup.

Specific Comment #5

*Page 2-4, Section 2.4, 2nd paragraph:* *The paragraph cites "Stanley Consultants, 2014" to support the observations of the lithology of the Muddy Creek Formation. Please add a full citation in the references section.*

Specific Comment #5 Response

The citation "Stanley Consultants, 2014" was added to the reference section.

Specific Comment #6

*Page 2-4, Section 2.4, 2nd paragraph:* *The last sentence in the paragraph states "Split spoon samples will be collected during drilling to identify the lithology." Please add a discussion of what depth intervals samples are anticipated to be collected and state if split spoon samples will be collected within the anticipated screened interval of the well.*

Specific Comment #6 Response

The initial plan was to use hollow stem auger drilling technology to install the monitoring well. Since this monitoring well will be installed during other drilling activities it was decided that using Sonic drilling technology would be more cost effective. The text in the work plan has been edited to reflect this change.

Specific Comment #7

*Page 2-5, Section 2.4, 1st paragraph:* *Please add a description of the methodology and materials anticipated to be used to plug the borehole back from the top of the Muddy Creek Formation to the bottom of the proposed screened interval.*

Specific Comment #7 Response

After the confirmation of the top of the Muddy Creek Formation, the bore hole will be filled with bentonite chips to the bottom of the screened interval.

Specific Comment #8

*Page 4-1, Section 4.1, Field Variances:* *This work plan is in the review stage; however, prior to work plan finalization, some soil sampling has been completed. The work completed to date was approved by NDEP in 2015. A brief discussion of the work completed and the NDEP review should be included either in Section 4 or in another section of NVE's choosing*

Specific Comment #8 Response

The following wording was added to page 2-2 "NV Energy completed preliminary soil sampling in December 2015 with completion scheduled by mid-2016. Laboratory soil data will be provided and summarized in a future deliverable".

Specific Comment #9

*Page 4-1, Section 4.1, Field Variances:* *Last sentence- Please add "Additionally, NDEP will be notified at least 14 days prior to the initiation of monitoring well installation activities."*

Specific Comment #9 Response

The following statement was added "Additionally, NDEP will be notified at least 14 days prior to the initiation of monitoring well installation activities."

Specific Comment #10

*Page 6-1, Section 6, Table 6-1:* *The text in the second column, third row appears to need revision. Do you mean "Following well development in September 2016?"*

Specific Comment #10 Response

The following statement was added "Following well development **in** September 2016."

Specific Comment #11

*Figure 2:* *The soil sampling locations do not appear to accurately reflect where surface soil samples were collected, although the proposed well location appears to accurately reflect the current location agreed upon by NVE and NDEP. Please correct the map to accurately reflect the current information for the site.*

Specific Comment #11 Response

Figure 2 showing the sample locations was not revised because the actual sample locations are shown on Figure 2.

Specific Comment #12

| |
|---|
| *<u>Figure 2:</u> Please provide additional discussion in the attached table as to the purpose of soil sample B6 (also comment 2b, above). Please amend the table to better describe the reasoning associated with this sample.* |

Specific Comment #12 Response

| |
|---|
| The table in figure 2 has been amended to read “The additional sample location (B-6) may be needed in order to conduct a statistical evaluation should there be impacts from the first mobilization. At least 12 total soil samples are needed to conduct a statistical evaluation using the EPA software ProUCL to determine the 95% Upper Confidence Limit (UCL). If the calculated 95% UCL is at or below the BCLs and BTVs, then the area needs no further investigation or cleanup.” |

---

**Final**

To NDEP — From NV Energy

Submittal Date March 2016 — Comment Date 3/18/2016

Response Date 4/7/2016

Commenter Alison Oakley — Responder Jason Reed

Comment #1

| |
|---|
| *<u>Page 2-2, Section 2.3, first full paragraph of page:</u>*<br><br>*Please clarify which version of ProUCL will be used. Will ProUCL be run for all distributions, or a selection of distributions? Please clarify how will non-detects be treated.* |

Comment #1 Response

| |
|---|
| Page 2-2 and Footnote 5 on Page 2-4 were revised to state the following:<br><br>“At least 12 total soil samples are needed to conduct a statistical evaluation using the EPA software ProUCL Version 5.0.00 (EPA, 2013) to determine the 95% Upper Confidence Limit (UCL). The UCL calculation will include non-detect values and will be determined for all distributions provided for in the software (normal, lognormal, gamma, and non-parametric). Non-detect data will be entered as ½ the detection limit. If the calculated 95% UCL is at or below the BCLs and BTVs, then the area needs no further investigation or cleanup. During the second mobilization a monitoring well will be installed. If soil samples collected during the first mobilization do not exceed screening levels, the excavation will be backfilled.” |

Comment #2

| |
|---|
| *<u>Page 7-1, Section 7:</u>*<br><br>*Please add the full citation for the version of ProUCL that will be used to evaluate the data.* |

Comment #2 Response

| |
|---|
| The following reference was added to Page 7-1, Section 7:<br><br>EPA, 2013. Statistical Software ProUCL 5.0.00 for Environmental Applications for Data Sets with and without Nondetect Observations, https://www.epa.gov/land-research/proucl-software. September, 2013. |

<u>Additional revisions:</u>
The objectives listed in Section 5 have been added to Section 1, and additional minor editorial changes have been made throughout the document.

# SA-8 Groundwater and Soil Characterization Work Plan Administrative Order on Consent Activities

**NV Energy**
Reid Gardner Station

**Final**
April 2016
20618.09.44

# Certifications

## NV Energy Certification

I certify that this document and all attachments submitted to the Division were prepared under the direction or supervision of NV Energy in accordance with a system designed to gather and evaluate the information by appropriately qualified personnel. Based on my inquiry of the person or persons who manage the system(s) or those directly responsible for gathering the information, or the immediate supervisor of such person(s), the information submitted and provided by NV Energy is, to the best of my knowledge and belief, true, accurate, and complete in all material respects. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Signature: [signature]
Name: Jason Hammons
Title: Plant Director, Reid Gardner Station
Company: NV Energy
Date: 4/7/16

# Certified Environmental Manager Certification

I hereby certify that I am responsible for the services described in this document and for the preparation of this document. The services described in this document have been provided in a manner consistent with the current standards of the profession and to the best of my knowledge comply with all applicable federal, state and local statutes, regulations and ordinances.

Signature: [signature]
Name: Jonathan Sarich
Title: Environmental Scientist
Company: Stanley Consultants
Date: 4/7/2016
EM Certificate Number: EM-2361
EM Expiration Date: 9/25/2017

# Table of Contents

## TABLES



## APPENDICES

# Section 1

# Introduction and Background

This SA-8 Groundwater and Soil Characterization Work Plan (Work Plan) is being submitted to the Nevada Division of Environmental Protection (NDEP) Bureau of Corrective Action (BCA) to evaluate the nature and extent of contamination associated with this source area (Station Source Area SA-8), as part of the Administrative Order on Consent (AOC) for the Reid Gardner Station (Station) signed by Nevada Power Company (NPC) dba NV Energy and NDEP on February 22, 2008 (NDEP and NV Energy, 2008).

The Station is a coal-fired electric power generation facility. The Station is located approximately 45 miles northeast of Las Vegas, within the Moapa Valley. The Station was developed in 1964 and the Station became commercially operational in 1965. Generating Units 1, 2, and 3 were permanently taken offline by NV Energy in December 2014, Unit 4 is currently operational and is scheduled to be removed from service in December 2017.

The former Unit 1,2,3 Catch Basin (CTCB) was formally removed from service in the fourth quarter of 2014 when the associated cooling towers were demolished by NV Energy. The concrete lined basin with associated pumps and piping were demolished and disposed of offsite in December 2015. This work plan focuses on characterization of the soil and groundwater underlying the former concrete lined catch basin. Figure 1 in Appendix A shows a layout of the site and the location of the former CTCB.

## 1.1 Objectives

The objectives of this Work Plan are to evaluate the nature and extent of contamination associated with this source area and to:

1. Characterize potential secondary source beneath the former CTCB.
2. Gather information to support possible future groundwater modeling efforts.
3. Gather information to support corrective action planning.

4. Gather data to contribute to development of the Site-wide Conceptual Site Model (CSM).

This Work Plan describes the history, background, and current conditions associated with the former CTCB. Also discussed are soil and groundwater sampling, quality control, data evaluation, and reporting procedures to be implemented during the course of this work.

## 1.2 Background

The former CTCB was originally constructed in 1976 (NPC, 1976) to contain stormwater runoff and cooling tower overflow (Stanley Consultants, 2013). Solids that collected in the pond during plant operations were periodically removed and placed in the on-site landfill.

The former CTCB was first investigated as part of a Phase I Environmental Site Assessment (ESA) completed by CH2M Hill in 1998 (CH2M Hill, 1998). One pond water and sediment sample were collected during a Supplemental Phase II ESA performed by Kleinfelder in 2000 (Kleinfelder, 2000). The pond water data does not show parameters present at levels of concern other than arsenic slightly above the primary maximum contaminant level (MCL) and aluminum, magnesium and total dissolved solids (TDS) above the secondary MCL. The sediment sample was analyzed for the eight Resource Conservation and Recovery Act (RCRA) metals by the toxicity characteristic leaching procedure (TCLP) method. All constituents in the sediment sample were below the EPA regulatory limits for TCLP metals. Barium was reported at 0.46 milligrams per liter (mg/L) and other metals were below method detection limits. No soil or groundwater samples were collected and analyzed as part of the Kleinfelder’s Phase II ESA.

# Section 2

# Field Investigations

The Work Plan includes subsurface investigations (soil and groundwater) in the former CTCB area. Utility clearance will be conducted prior to initiation of any intrusive drilling activities.

## 2.1 Investigation Team

Stanley Consultants will be responsible for coordinating the implementation of this Work Plan. Utility clearance and drilling/monitoring well installation will be performed by others contracted by NV Energy. NV Energy will survey the monitoring well and soil boring locations installed as part of this Work Plan. Veritas Laboratories (and subcontracted laboratories) will perform laboratory analyses and data validation will be performed by Ordway and Associates, a subcontractor to Stanley Consultants. OGI will collect groundwater samples from the newly installed monitoring well as part of the second semi-annual groundwater monitoring event in September 2016.

## 2.2 Utility Clearance

The monitoring well location will be air-knifed to a depth of six feet below ground surface (bgs) prior to the initiation of any intrusive drilling activities (i.e., Sonic drilling). The drilling contractor hired by NV Energy will be responsible for performing a utility clearance for all proposed boring locations, calling each drilling location into the North Underground Service Alert, and meeting with relevant utility service staff in the field, if needed, to clear individual boring locations. The drilling contractor will also be responsible for obtaining all necessary work permits (i.e., drilling, dust permit, well installation, etc.).

## 2.3 Surface Soil Sampling

Surface soil samples will be collected using a decontaminated stainless-steel trowel at the locations illustrated on Figure 2 in Appendix A and summarized in Table 2-1. The samples will then be placed in a cooler with ice, closed with custody seals and delivered to Veritas Laboratories under standard chain-of-custody.

Field work will be completed in two mobilizations. During the first mobilization five soil samples will be collected at depths of 0.0 – 0.5 feet. If laboratory results from the first mobilization indicate soil contamination exceeding the Environmental Protection Agency (EPA) Region 9 risk-based screening levels (RSLs) (EPA, 2015) for industrial soil then a second mobilization will be required to define the extent of contamination. If there is not an EPA RSL, then the analytical results will be compared to the site-specific background threshold values (BTVs) or the NDEP Basic Contaminant levels (BCLs). The results will be first compared to the EPA RSL, if there is no EPA RSL for a specific analytical result then the result will be compared to the site-specific BTVs or BCLs. If a second round of soil samples is needed the samples will be collected at depths 2-3 feet below ground surface at the same locations as the soil samples collected during the first mobilization. The additional sample location (B-6) may be needed in order to conduct a statistical evaluation should there be impacts from the first mobilization. At least 12 total soil samples are needed to conduct a statistical evaluation using the EPA software ProUCL Version 5.0.00 (EPA, 2013) to determine the 95% Upper Confidence Limit (UCL). The UCL calculation will include non-detect values and will be determined for all distributions provided for in the software (normal, lognormal, gamma, and non-parametric). Non-detect data will be entered as ½ the detection limit. If the calculated 95% UCL is at or below the BCLs and BTVs, then the area needs no further investigation or cleanup. During the second mobilization a monitoring well will be installed. If soil samples collected during the first mobilization do not exceed screening levels, the excavation will be backfilled.

Sampling activities and analytical methods will be conducted following guidance included in the NDEP approved Quality Assurance Project Plan (QAPP) (Stanley Consultants, 2011). The soil samples collected will be analyzed for, the indicator constituents of concern approved by NDEP on December 16, 2015 (Appendix B), Antimony, Arsenic, Boron, Cadmium, Chloride, Chromium, Fluoride, Molybdenum, Phosphorous, Selenium, Sodium, Sulfate, Thallium, and TDS (groundwater only), and Polynuclear Aromatic Hydrocarbons (PAHs).

NV Energy completed preliminary soil sampling in December 2015 with completion scheduled by mid-2016. NV Energy provided preliminary laboratory soil data results to NDEP on March 21, 2016.

**Table 2-1**

**SA-8 Soil and Groundwater Sampling**

| Boring | Target Soil Sample Depth (feet below pond bottom) | 1st Mobilization | 2nd Mobilization |
|---|---|---|---|
| SA-8-B1 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | 1 soil sample (If laboratory results from 1st mobilization indicate potential soil contamination) |
| SA-8-B2 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | 1 soil sample (If laboratory results from 1st mobilization indicate potential soil contamination) |
| SA-8-B3 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | If laboratory results from 1st mobilization indicate potential soil contamination, one soil sample will also be collected at this depth |
| SA-8-B4 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | If laboratory results from 1st mobilization indicate potential soil contamination, one soil sample will also be collected at this depth |
| SA-8-B5 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | 1 soil sample (If laboratory results from 1st mobilization indicate potential soil contamination) |
| SA-8-B6 | 0.0-0.5 | | 1 soil sample (if laboratory results from 1st mobilization indicate potential soil contamination) |
| | 2-3 | | 1 soil sample (if laboratory results from 1st mobilization indicate potential soil contamination) |
| SA-8-MW-1 | | | 1 groundwater sample. Sonic boring will tag top of Muddy Creek Formation, estimated at 50' bgs. Well will be screened from 15'-25' bgs |

Notes:

1) Depth of sample collection subject to change based on field conditions.
2) All samples will be collected in accordance with the NDEP-approved QAPP.
3) Soil data will be compared with site-specific background levels and EPA Region 9 risk-based screening levels. Soil may be considered contaminated if concentrations exceed one or both of these screening levels.
4) If soil samples collected during the first mobilization do not exceed screening levels, excavation will be backfilled.
5) If one or more of the soil concentrations from the first mobilization exceed site-specific background and/or EPA Region 9 risk-based screening levels, additional soil samples will be collected during the second mobilization. At least 12 total soil samples are needed to conduct a statistical evaluation using the 95% UCL. The additional sample location (B-6) may be needed in order to conduct a statistical evaluation should there be impacts from the first mobilization. At least 12 total soil samples are needed to conduct a statistical evaluation using the EPA software ProUCL Version 5.0.00 (EPA, 2013) to determine the 95% Upper Confidence Limit (UCL). The UCL calculation will include non-detect values and will be determined for all distributions provided for in the software (normal, lognormal, gamma, and non-parametric). Non-detect data will be entered as ½ the detection limit. If the calculated 95% UCL is at or below the BCLs and BTVs, then the area needs no further investigation or cleanup.
6) Laboratory parameters are the indicator constituents of concern approved by NDEP on May 6, 2015: Antimony, Arsenic, Boron, Cadmium, Chloride, Chromium, Fluoride, Molybdenum, Phosphorous, Selenium, Sodium, Sulfate, Thallium, and Total Dissolved Solids (groundwater only) plus the following PAHs that could be present in stormwater runoff: Acenaphthene, anthracene, benzo(a)anthracene, benzo(a)pyrene, benzo(b)fluoranthene, benzo(g,h,i)perylene, benzo(k)fluoranthene, bis(2-ethylhexyl)phthalate, chrysene, fluoranthene, fluorine, indeno(1,2,3-cd)pyrene, naphthalene, phenanthrene, pyrene, and 1,1-byphenyl.
7) Based on a review of Material Safety Data Sheets, the following chemicals were components of cooling tower additives: tolytriazole, tri-n-butyl oxide, chlorinated hydantoins, morpholine, hydroquinone, and methoxypropylamine. These parameters were identified as ones with no Nevada certified laboratories to provide the analysis. NDEP indicated in a letter dated October 13, 2009 that they concur with NV Energy's August 27, 2009, request to not sample for these parameters.

## 2.4 Monitoring Well Installation

One monitoring well will be installed using Sonic drilling technology in accordance with ASTM D6914-04, Standard Practice for Sonic Drilling for Site Characterization and the Installation of Subsurface Monitoring Devices. Sonic drilling will allow field geologists to observe continuous soil cores, which will be lithologically logged by the Unified Soil Classification System (USCS) in accordance with ASTM D2488.

The boring will be completed to a depth where the top of the Muddy Creek Formation can be confirmed by visual inspection by the field geologist. The upper portion of the Muddy Creek Formation at the Station has been described as being a massive (several feet thick) reddish brown, very stiff, hard, dry, lean clay, non-cohesive and non-plastic, with gypsum crystals or pods. Beneath the upper clay layer are thin to massive beds of very fine well graded, loose, saturated sand (sugar sand) (Stanley Consultants, 2014). At some locations, particularly in the plant site, the contact between the alluvium and the underlying Muddy Creek Formation has been marked by a thin (<1 foot) cemented sandstone layer (NTL, 1980). The top of the Muddy Creek Formation is estimated to be at approximately 50 feet bgs based on neighboring borings at former Pond 4A and the Raw Water Ponds. The Muddy Creek Formation can be distinguished visually from the overlying Quaternary Alluvium which is described in neighboring soil boring logs as brown to gray interbedded, poorly sorted very coarse to fine sand, silt, and soft to stiff clay with varying amounts of fine to coarse gravel and cobbles. The individual alluvial layers range from a few inches to several feet thick. Based on previous subsurface investigations at the Station, flowing sands may be encountered during drilling activities. After the confirmation of the top of the Muddy Creek Formation, the bore hole will be filled with bentonite chips to the bottom of the screened interval.

The drilled boring will be completed with a four-inch-diameter groundwater monitoring well per ASTM-D5092-04, Standard Practice for Design and Installation of Ground Water Monitoring Wells (see Appendix C), with a minimum of 1 foot of threaded schedule 40 polyvinyl chloride (PVC) #10 (0.01 inch) slotted screen, a threaded end plug or point, and an expandable locking cap. Well casing will be threaded schedule 40 PVC with "O-rings" between five- and ten-foot lengths. The well will be screened across the upper-most water bearing zone interface with approximately 5 feet of screen extending above and ten feet below the water table surface observed during drilling activities. The PVC will extend to three feet above the ground surface for an aboveground completion. The annular space around the well screen will be backfilled with #12 silica sand to two feet above the top of the screen. A sanitary seal comprised of a minimum of two feet of hydrated bentonite chips or pellets will be installed on top of the sand. A bentonite grout slurry will be installed on top of the seal and extend to the upper two feet of the schedule 40 PVC riser pipe. A concrete cap will be placed around the pipe to keep the pipe from sinking. The grout will be allowed to cure and settle for 72 hours prior to installing the concrete surface seal and protective steel casing. If necessary, additional grout will be added to the borehole to return the level to within two feet of the ground surface. Stainless steel centralizers will be used to keep the well in the middle of the borehole during construction. The aboveground well completion will be finished with a locking outer protective steel casing concreted into place, with three bollards placed around the well for protection.

The proposed groundwater monitoring well will be developed after installation in accordance with standard operating procedure (SOP) 2044 in Appendix E of the NV Energy QAPP.

## 2.5 Groundwater Elevation Measurement

The groundwater level will be manually measured in the well after development and on a quarterly basis, starting with the first subsequent groundwater monitoring event. The groundwater level will be measured with an electronic water level meter in accordance with SOP 2043 in Appendix E of the NV Energy QAPP.

## 2.6 Groundwater Sampling

Following well development activities, an initial measurement of field pH, specific conductance, temperature, and water level will be recorded, and a groundwater sample collected for laboratory analysis. As part of this Work Plan, a second set of groundwater samples will be collected during the subsequent groundwater monitoring events. Table 2-1 shows the parameters and methods for the field and laboratory analyses. Sampling procedures are specified in Section B2 of the NV Energy QAPP.

After completion of the groundwater elevation measurements, all wells will be purged prior to sampling in accordance with the NV Energy QAPP. At each sampling location, all bottles designated for a particular analysis will be filled sequentially before bottles designated for the next analysis are filled in accordance with the NV Energy QAPP. Groundwater samples will be transferred from the tubing directly into the appropriate sample containers with preservative, if required, chilled if appropriate, and processed for shipment or delivery to the laboratory. When transferring samples, care will be taken not to touch the tubing to the sample container.

## 2.7 Sample Containers, Preservation, and Storage

Veritas Laboratories will provide the appropriate sample containers and preservatives for all groundwater and soil sampling events. The sample containers, preservation, and storage will be as specified in Table 3 in Section B2 of the NV Energy QAPP and per Section 3.0 of the Veritas Quality Assurance Quality Control Plan in Appendix C of the NV Energy QAPP.

## 2.8 Surveying

The location of the newly-installed monitoring well will be surveyed by NV Energy surveyors consistent with the previous monitoring well surveying at the Station. In addition to surveying the horizontal and vertical locations, the ground surface and north side of the top of PVC casing at the well will be surveyed to determine the respective elevations. The top of casing elevation will then be used to determine groundwater elevations. All surveying will tie into the existing site coordinate system and the data will be provided electronically by the surveyors so it can be integrated into the AOC Geographic Information System (GIS).

## 2.9 Field Documentation

All documentation of field activities will be as specified in Section A9.0 of the NV Energy QAPP. Sample handling and shipment will be as specified in Section B3.0 and detailed in Appendix E of the NV Energy QAPP. Field data will be recorded in the logbook, on field activity forms, and/or electronically. Photographs of field activities will be taken and included in the SA-8 Groundwater and Soil Characterization Implementation Report.

## 2.10 Decontamination

All equipment that comes into contact with soil and groundwater will be decontaminated prior to each use in accordance with the EPA Region 9 decontamination procedures referenced in Appendix E of the NV Energy QAPP. Where practical, disposable equipment will be used and will not be decontaminated.

## 2.11 Investigation Derived Waste

Investigation-derived waste will be disposed in accordance with applicable regulations. Soil cuttings will be screened with a photoionization detector (PID) and if less than 100 parts per million (ppm) the cuttings will be temporarily containerized and then disposed of in NV Energy’s onsite landfill in accordance with the Southern Nevada Health District (SNHD) permit. Well development and decontamination water will be containerized and disposed in the onsite evaporation ponds in accordance with NV Energy’s Authorization to Discharge permit. Decontamination chemicals such as non-phosphate detergent and deionized (DI) water will be collected and containerized as described in SOP 2006 Appendix E of the NV Energy QAPP.

# Section 3

# Quality Control

Quality control (QC) measures will be conducted in accordance with the NV Energy QAPP. The collection of QC samples (e.g., equipment blanks, duplicate samples, etc.) as well as the data validation process is discussed below.

## 3.1 Quality Control Samples

In accordance with Table 4 in Section B5.2 of the NV Energy QAPP, the QC requirements pertaining to soil and water samples collected for laboratory analysis are listed in Table 3-1. The frequency of these activities will be based on the combined field activities occurring at any given time during the implementation of the Work Plan.

**Table 3-1**

**QC Sampling and Analysis Summary**

| AOC Implementation Activity | Organization | Frequency of Activity |
|---|---|---|
| Field Blank | Stanley Consultants /OGI | 1 per day or 5% of primary field samples (whichever is less) as specified in Section B5.2.2.1 of the QAPP |
| Equipment Rinsate Blank | Stanley Consultants /OGI | 1 per day or 5% of primary field samples (whichever is less) as specified in Section B5.2.2.1 of the QAPP |
| Blind Field Duplicate Sample | Stanley Consultants /OGI | 1 per day, per medium, per analytical method as specified in Section B5.2.2.3 of the QAPP. No duplicate samples required for soil samples |

**Table 3-1**

**QC Sampling and Analysis Summary (continued)**

| AOC Implementation Activity | Organization | Frequency of Activity |
|---|---|---|
| Trip Blank | Stanley Consultants /OGI<br>Veritas Laboratories | Not applicable – no volatile organic analyses |
| Lab Reagent Blank | Veritas Laboratories | As specified in Appendix C of the QAPP |
| Method Blank | Veritas Laboratories | As specified in standard method SOP, Appendix C of the QAPP |
| Matrix Spike/Matrix Spike Duplicate | Veritas Laboratories | As specified in standard method SOP, Appendix C of the QAPP |
| Lab Control Sample | Veritas Laboratories | As specified in Appendix C of the QAPP |
| General Bottle Control | Veritas Laboratories | Certified by Manufacturer |

During the Groundwater and Soil Characterization sampling events, blanks and duplicate samples will be collected in accordance with the NV Energy QAPP and Table 3-1. Sampling locations will be documented in the field logbook and/or on the Field Summary Forms in Appendix D of the NV Energy QAPP. Field blanks will be used to check for analytical artifacts and/or site background contaminants introduced by sampling, transportation, and analytical procedures. These QC samples will be collected by pouring laboratory-provided DI water into sample containers provided by Veritas Laboratories in the area of the field investigations.

Equipment or rinsate blanks will be used to check field decontamination procedures and will be collected by pouring laboratory-provided DI water through a sampling device after decontamination. If the sampling equipment (i.e., disposable bailer) is certified contaminant-free by the manufacturer, equipment blanks will not be collected during the use of that device.

Field duplicate samples will be used to evaluate the variance of the sampling and laboratory analysis methods. These QC samples will be collected by the same procedures and at the same time as the corresponding primary field sample in accordance with the NV Energy QAPP. The primary and duplicate samples will be assigned different (unique) sample identifiers (i.e., Sample IDs) that do not indicate to the laboratory that they are duplicate samples. No duplicate samples are required for soil samples.

## 3.2 Field Equipment Calibration

Field equipment will be calibrated as shown in Table 3-2. The frequencies meet the minimum requirements specified by the equipment manufacturer, industry SOPs, and EPA guidance.

**Table 3-2**

**Field Equipment Calibration Frequency**

| Field Instrument | Calibration Checks | |
|---|---|---|
| | **Pre-Field Bench Check at Mobilization** | **On-Site** |
| Temperature/pH Meter | X | Daily or if conditions change |
| Specific Conductance meter | X | Daily or if conditions change |

## 3.3 Data Usability/Validation

Data from all soil and groundwater samples collected for laboratory analyses will be submitted to Ordway and Associates for third party data validation and usability determination. Stage 2B and 4 data validation will be conducted in accordance with the Revised Data Validation Memorandum of Understanding dated March 5, 2010 and approved by the NDEP on March 10, 2010, as provided in the NV Energy QAPP.

If soil samples collected during the first mobilization do not exceed EPA RSLs, the excavation will be backfilled and compacted with clean fill materials from an off-site source.

# Section 4

# Field Variances

During the implementation of the SA-8 Groundwater and Soil Characterization Work Plan, it may be necessary to make minor modifications to the planned activities in the field as conditions change. If the selected alternative is deemed to have no significant impact on the investigation objectives, it will be implemented and documented in the SA-8 Groundwater and Soil Characterization Report. However, if the modification is deemed to have a potentially significant impact on the investigation objectives, work will stop until the NDEP or their representative can be consulted regarding the changes. If concurrence with the modifications to the SA-8 Groundwater and Soil Characterization Work Plan cannot be reached, NV Energy may decide to proceed at risk knowing that NDEP may not agree to use of the data for decision making purposes.

All modifications to the NDEP-approved SA-8 Groundwater and Soil Characterization Work Plan will be documented and discussed in the SA-8 Groundwater and Soil Characterization Report.

NV Energy completed preliminary soil sampling in December 2015 with completion scheduled by mid-2016. Laboratory soil data will be provided and summarized in a future deliverable. In accordance with the AOC, NDEP will be notified at least 14 days prior to conducting sampling activities outlined in this Work Plan. Additionally, the NDEP will be notified at least 14 days prior to the initiation of monitoring well installation activities.

# Section 5

# Data Evaluation and Reporting

This section explains how the data collected during the implementation of the PA3 Groundwater and Soil Characterization Work Plan will be evaluated to address the objectives presented in Section 1 (objectives are listed in italics). In addition, a data management approach is provided to describe how the data will be compiled, reviewed and reported.

## 5.1 Data Evaluation

1. *Characterize potential secondary source beneath the former CTCB.* The potential secondary source will be characterized by analyzing soil samples collected beneath the CTCB and comparing the results to the Region 9 RSLs.
2. *Gather information to support possible future groundwater modeling efforts.* All of the data collected will support future groundwater modeling efforts because it will inform the Site-wide CSM. For example, the geologic information will be used to define the depth of the alluvial aquifer. The groundwater elevation data from new and existing wells will be important for setting up and calibrating a model.
3. *Gather information to support corrective action planning.* All of the information collected to support previous objectives will also be used to evaluate whether corrective action is needed to protect potential receptors and, if so, what types of corrective action approaches might be feasible for the CTCB Area.
4. *Gather data to contribute to development of the Site-wide CSM.* All of the data from this investigation will be used to strengthen the Site-wide CSM.

# Section 6

# Schedule

NV Energy began the Units 1,2,3 CTCB Groundwater and Soil Characterization field activities in December 2015 with the drilling activities scheduled to be completed in May 2016. The second semi-annual groundwater sampling event is scheduled for September 2016. In accordance with the AOC, NDEP will be notified at least 14 days prior to conducting sampling activities outlined in this Work Plan. The tentative schedule of field activities proposed in this Work Plan is presented in Table 6-1 below.

**Table 6-1**

**Proposed Field Activities Schedule**

| Activity | Field Schedule | Locations |
|---|---|---|
| Soil Sampling | December 2015 | SA-8-B1, SA-8-B2, SA-8-B3, SA-8-B4, SA-8-B5 at a depth of 0.0-0.5 feet |
| Drilling, Soil Sampling, Well Installation, Groundwater Sampling and Surveying | April/May 2016 | SA-8-B1, SA-8-B2, SA-8-B3, SA-8-B4, SA-8-B5, SA-8-B6 (if required at depth 2-3 feet) SA-8-MW-1 |
| Groundwater Elevation Measurement and Sampling | Following well development in September 2016 | SA-8-MW-1 |

# Section 7

# References


CH2M Hill, 1998. *Phase I Environmental Site Assessment*, October 1998.

EPA, 2013. *Statistical Software ProUCL 5.0.00 for Environmental Applications for Data Sets with and without Nondetect Observations*, https://www.epa.gov/land-research/proucl-software. September, 2013.

EPA, 2015. Regional Screening Level (RSL) Summary Table, Generic Tables. (http://www.epa.gov/region9/superfund/prg/). December 2015.

Kleinfelder, 2000. *Supplemental Phase II Environmental Site Assessment Task Reports*, June 2000.

NDEP and NV Energy, 2008. *Nevada Division of Environmental Protection, Administrative Order on Consent (AOC),* February 22, 2008.

NPC, 1976. *Unit Number 3*, March 1976.

NTL, 1980. Nevada Testing Laboratories, *Report of Soils Investigation*, Contract RG-205, Reid Gardner Station, Unit 4, Nevada Power Company, NTL Lab No. 2860S, March 10, 1980.

Stanley Consultants, 2011. *Generic Quality Assurance Project Plan, AOC Implementation Activities, Version 2.5*, November 2015.

Stanley Consultants, 2013. *Preliminary Source Area Identification and Characterization Report*, July 2013.

Stanley Consultants, 2014. *Background Conditions Report,* NV Energy, Reid Gardner Station, Moapa, Nevada, Draft, December 2014.

# Section 8

# Acronyms and Abbreviations

| | |
|---|---|
| AOC | Administrative Order on Consent |
| BCA | Bureau of Corrective Action |
| BCL | Background Contaminant Level |
| bgs | Below ground surface |
| BTV | Background Threshold Value |
| CSM | Conceptual Site Model |
| CTCB | Catch Basin |
| dba | doing business as |
| DI | Deionized water |
| EPA | Environmental Protection Agency |
| ESA | Environmental Site Assessment |
| GIS | Geographic Information System |
| mg/L | milligrams per liter |
| MCL | Maximum Contaminant Level |
| NDEP | Nevada Division of Environmental Protection |
| NPC | Nevada Power Company |
| PAHs | Polynuclear Aromatic Hydrocarbons |
| PID | Photoionization detector |
| PVC | Polyvinyl Chloride |
| QAPP | Quality Assurance Project Plan |
| QC | Quality control |
| RCRA | Resource and Conservation Act |
| RSL | Regional Screening Level |
| SNHD | Southern Nevada Health District |
| SOP | Standard Operating Procedure |
| Station | Reid Gardner Station |
| TCLP | Toxicity Characteristic Leaching Procedure |
| TDS | Total Dissolved Solids |
| UCL | Upper Confidence Limit |
| USCS | Unified Soil Classification System |

# Appendix A

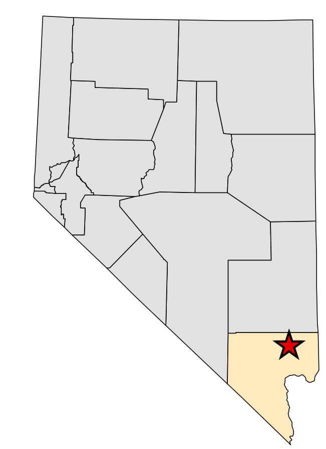
# Figures


**Legend**

- SA-8 Outline
- Existing Pond
- Property Boundary
- Muddy River

1,000 500 0 1,000 2,000 Feet

Notes:
1. Aerial imagery provided by Clark County Assessor Office; photographs taken Spring 2013



Stanley Consultants INC.

March 2016

SA-8 LOCATION
UNITS 1,2,3 CATCH BASIN
AOC Implementation
NV Energy
Reid Gardner Station
Moapa, NV
Figure 1

| REV | No. | REVISION DESCRIPTION | DATE | DRWN | CHKD | APVD |
|---|---|---|---|---|---|---|
| | | | | | | |
| | | | | | | |
| | | | | | | |
| 1 | | Submittal to NDEP | 3/3/16 | CC | JS | BC |
| 0 | | Submittal to NDEP | 2/5/16 | CC | JS | BC |

0 1in.
At full size
1 inch = 1,000 feet

NVEnergy

20618.09.44

REV.
1

\\lcy-fs1\Projects_F\20618_03_NVE_RGS_AOC_Imp09\Active\14-GIS\GIS\WorkingData\Mxd\SA8\SA-8_CatchBasin_SiteMap.mxd © STANLEY CONSULTANTS


**SA-8 Soil and Groundwater Sampling**

| Boring | Target Soil Sample Depth (feet below pond bottom) | 1st Mobilization | 2nd Mobilization |
|---|---|---|---|
| SA-8-B1 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | 1 soil sample (If laboratory results from 1st mobilization indicate potential soil contamination). |
| SA-8-B2 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | 1 soil sample (If laboratory results from 1st mobilization indicate potential soil contamination). |
| SA-8-B3 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | If laboratory results from 1st mobilization indicate potential soil contamination, one soil sample will also be collected at this depth. |
| SA-8-B4 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | If laboratory results from 1st mobilization indicate potential soil contamination, one soil sample will also be collected at this depth. |
| SA-8-B5 | 0.0-0.5 | 1 soil sample | |
| | 2-3 | | 1 soil sample (If laboratory results from 1st mobilization indicate potential soil contamination). |
| SA-8-B6 | 0.0-0.5 | | 1 soil sample (if laboratory results from 1st mobilization indicate potential soil contamination). |
| | 2-3 | | 1 soil sample (if laboratory results from 1st mobilization indicate potential soil contamination). |
| SA-8-MW-1 | | | 1 groundwater sample. Hollow stem auger boring will tag top of Muddy Creek Formation at about 50' bgs. Well will be screened at 15-25' bgs. |

**Table Notes:**
**1)** Depth of sample collection subject to change based on field conditions.
**2)** All samples will be collected in accordance with the NDEP-approved Quality Assurance Project Plan (QAPP).
**3)** Soil data will be compared with EPA Region 9 risk-based screening levels for industrial soil.
**4)** If soil samples collected during the first mobilization do not exceed screening levels, excavation will be backfilled.
**5)** Laboratory parameters are the indicator constituents of concern approved by NDEP on May 6, 2015: Antimony, Arsenic, Boron, Cadmium, Chloride, Chromium, Fluoride, Molybdenum, Phosphorus, Selenium, Sodium, Sulfate, Thallium, and Total Dissolved Solids (groundwater only) plus the following PAHs that could be present in stormwater runoff Acenaphthene, anthracene, benzo(a)anthracene, benzo(a)pyrene, benzo(b)fluoranthene, benzo(g,h,i)perylene, benzo(k)fluoranthene, bis (2-ethylhexyl)phthalate, chrysene, fluoranthene, fluorene, indeno(1,2,3-cd)pyrene, naphthalene, phenanthrene, pyrene, and 1,1-biphenyl.
The additional sample location (B-6) may be needed in order to conduct a statistical evaluation should there be impacts from the first mobilization. At least 12 total soil samples are needed to conduct a statistical evaluation using the EPA software ProUCL Version 5.0.00 (EPA, 2013) to determine the 95% Upper Confidence Limit (UCL). The UCL calculation will include non-detect values and will be determined for all distributions provided for in the software (normal, lognormal, gamma, and non-parametric). Non-detect data will be entered as ½ the detection limit. If the calculated 95% UCL is at or below the BCLs and BTVs, then the area needs no further investigation or cleanup.
During the second mobilization a monitoring well will be installed. If soil samples collected during the first mobilization do not exceed screening levels, the excavation will be backfilled.
**6)** Based on a review of Material Safety Data Sheets, the following chemicals were components of cooling tower additives: tolytriazole, tri-n-butyl oxide, chlorinated hydantoins, morpholine, hydroquinone, and methoxypropylamine. These parameters were identified as ones with no Nevada certified laboratories to provide the analysis. NDEP indicated in a letter dated October 13, 2009 that they concur with NV Energy's August 27, 2009, request to not sample for these parameters.

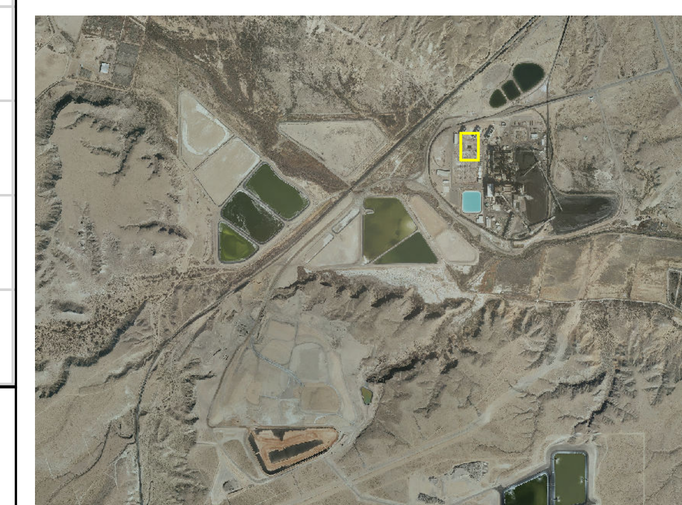
**Legend**

SA-8 Sampling Location
- Soil Boring
- Monitoring Well

N

50 25 0 50 100 Feet

Notes:
1. Aerial imagery provided by Clark County Assessor Office; photographs taken Spring 2013



Stanley Consultants INC.

March 2016

SA-8 SAMPLING LOCATIONS
UNITS 1, 2, 3 CATCH BASIN
AOC Implementation
NV Energy
Reid Gardner Station
Moapa, NV
Figure 2

| REV | No. | REVISION DESCRIPTION | DATE | DRWN | CHKD | APVD |
|---|---|---|---|---|---|---|
| | | | | | | |
| | | | | | | |
| 2 | | Submittal to NDEP | 3/29/16 | CC | JS | BC |
| 1 | | Submittal to NDEP | 3/3/16 | CC | JS | BC |
| 0 | | Submittal to NDEP | 2/5/16 | CC | JS | BC |

0 1in.
At full size
1 inch = 50 feet

NVEnergy

20618.09.44

REV.
2

\\cy-fs1\Projects_F\20618_03_NVE_RGS_AOC_Impl09\Active\14-GIS\GIS\WorkingData\Mxd\SA8\SA-8_CatchBasin_SamplingLocs.mxd © STANLEY CONSULTANTS

# Appendix B

# NDEP Letter

NEVADA DIVISION OF
**ENVIRONMENTAL PROTECTION**

**STATE OF NEVADA**
Department of Conservation & Natural Resources
Brian Sandoval, Governor
Leo M. Drozdoff, P.E., Director
Colleen Cripps, Ph.D., Administrator

May 6, 2015

Michael Rojo
Environmental Services, Supervisor
NV Energy
6226 W Sahara Ave M/S 30
Las Vegas, NV 89146

Re: **NV Energy (NVE)**
**Reid Gardner Station (RGS)**
**NDEP Facility ID #H-000530**
Nevada Division of Environmental Protection (NDEP) Comments and Concurrence with: *Request for Approval of Indicator Constituents of Concern for Reid Gardner Station AOC*

Dear Mr. Rojo:

The NDEP has received and reviewed NVE's *Request for Approval of Indicator Constituents of Concern for Reid Gardner Station AOC*. The letter, dated April 22, 2015, was received by the NDEP on April 29, 2015.

The letter requests that a subset of the Site Related Contaminants, which contains over 100 parameters, be used to develop the Conceptual Site Model (CSM). The reduced list of parameter is based on constituents that have been shown by the U.S. Environmental Protection Agency to be associated with coal-fired power plants and/or have been identified as specifically associated with the effluent discharge to the RGS evaporation ponds. The list of parameters is:

- Antimony,
- Arsenic,
- Boron,
- Cadmium,
- Chromium,
- Molybdenum,
- Selenium,
- Sulfate,
- Thallium,
- Total Dissolved Solids,
- Fluoride, and
- Phosphorus.

The last two parameters are included because the NDEP Bureau of Water Pollution Control lists the Muddy River as being "impaired" in the reach that flows through the Station. In addition to the twelve parameters listed above, the NDEP requests that sodium and chloride be included in the parameter list.

The NDEP concurs with the parameter list with the inclusion of sodium and chloride, for a total of fourteen indicator parameters. Please contact me with any questions or comments about this letter at (775) 687-9396 or aoakley@ndep.nv.gov

Sincerely,

Alison Oakley, CEM
Environmental Scientist III
Bureau of Corrective Actions
NDEP-Carson City Office

ec: Jeff Collins, Nevada Division of Environmental Protection (NDEP)
Scott Smale, Bureau of Corrective Actions, NDEP Carson City
Todd Croft, Bureau of Corrective Actions, NDEP Las Vegas
Bill Campbell, Tribal Liaison, NDEP
Alan Tiney, Bureau of Water Pollution Control, NDEP
Ebrahim Juma, Clean Water Team (ejuma@cleanwaterteam.com)
Joe Leedy, Clean Water Team (jleedy@cleanwaterteam.com)
Lynn M. Cintron, Southern Nevada Health District, (cintron@snhdmail.org)
Jacqueline Reszetar, Director of Envi. Health, Southern Nevada Health District reszetar@snhdmail.org
Brian Northam, Southern Nevada Health District, (northam@snhdmail.org)
Walter Ross, Environmental Health Supervisor/Engineer (Ross@snhdmail.org)
Andy Chaney, Southern Nevada Health District, (chaney@snhdmail.org)
Donna Houston, Southern Nevada Health District, (houston@snhdmail.org)
Starla Lacy, NV Energy (SLacy@nvenergy.com)
Don Hopper, NV Energy (DHopper@nvenergy.com)
Tony Garcia, NV Energy (TGarcia@nvenergy.com)
Michael Rojo, NV Energy (MRojo@nvenergy.com)
Jason Reed, NV Energy (JReed@nvenergy.com)
Becky Svatos, Stanley Consultants, Inc., (SvatosBecky@stanleygroup.com)
William Carrig, Stanley Consultants, Inc., (CarrigBill@stanleygroup.com)
John Kivett, ARCADIS U.S., Inc., (John.Kivett@arcadis-us.com)
Brad Cross, ARCADIS U.S., Inc., (Brad.Cross@arcadis-us.com)
Elliott Lips, Great Basin Earth Science, (elips@gbearthscience.com)
Andrea Issod, Sierra Club, (andrea.issod@sierraclub.org)
Robert Wiygul, Counsel Sierra Club and Moapa Band of Piutes, (Robert@waltzerlaw.com)
Ranajit Sahu, Consultant, (sahuron@earthlink.com)

cc: Alteha Tom, Moapa Band of Paiutes, Chairperson, P.O. Box 340, Moapa, NV 89025
Darren Daboda, Moapa Band of Paiutes, Environmental Director, P.O. Box 340, Moapa, NV 89025
Clark County Emergency Management, 500 S. Grand Central Parkway 6th Floor, P.O. Box 551713, Las Vegas, NV 89155-1713
Anitha Rednam, Department of Water Resources, 1416 9th Street, Room 1140, Sacramento CA 95814

# Appendix C

# ASTM Standards

Designation: D 5092 – 04[ε1]

# Standard Practice for Design and Installation of Ground Water Monitoring Wells[1]

This standard is issued under the fixed designation D 5092; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon (ε) indicates an editorial change since the last revision or reapproval.

ε[1] NOTE—Editorial changes were made throughout in June 2004.

## 1. Scope

1.1 This practice describes a methodology for designing and installing conventional (screened and filter-packed) ground-water monitoring wells suitable for formations ranging from unconsolidated aquifers (i.e., sands and gravels) to granular materials having grain-size distributions with up to 50 % passing a #200 sieve and as much as 20 % clay-sized material (i.e., silty fine sands with some clay). Formations finer than this (i.e., silts, clays, silty clays, clayey silts) should not be monitored using conventional monitoring wells, as representative ground-water samples, free of artifactual turbidity, cannot be assured using currently available technology. Alternative monitoring technologies (not described in this practice) should be used in these formations

1.2 The recommended monitoring well design and installation procedures presented in this practice are based on the assumption that the objectives of the program are to obtain representative ground-water samples and other representative ground-water data from a targeted zone of interest in the subsurface defined by site characterization.

1.3 This practice, in combination with proper well development (D 5521), proper ground-water sampling procedures (D 4448), and proper well maintenance and rehabilitation (D 5978), will permit acquisition of ground-water samples free of artifactual turbidity, eliminate siltation of wells between sampling events, and permit acquisition of accurate ground-water levels and hydraulic conductivity test data from the zone screened by the well. For wells installed in fine-grained formation materials (up to 50 % passing a #200 sieve), it is generally necessary to use low-flow purging and sampling techniques (D 6771) in combination with proper well design to collect turbidity-free samples.

1.4 This practice applies primarily to well design and installation methods used in drilled boreholes. Other Standards, including Guide D 6724 and Practice D 6725, cover installation of monitoring wells using direct-push methods.

1.5 The values stated in inch-pound units are to be regarded as standard. The values in parentheses are for information only.

1.6 *This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.*

1.7 *This practice offers a set of instructions for performing one or more specific operations. This document cannot replace education or experience and should be used in conjunction with professional judgment. Nat all aspects of this practice may be applicable in all circumstances. This ASTM standard is not intended to represent or replace the standard of care by which the adequacy of a given professional service must be judged, nor should this document be applied without consideration of a project's many unique aspects. The word "Standard" in the title of this document means only that the document has been approved through the ASTM consensus process.*

## 2. Referenced Documents

2.1 *ASTM Standards:* [2]

C 150 Specification for Portland Cement

C 294 Descriptive Nomenclature of Constituents of Natural Mineral Aggregates

D 421 Practice for Dry Preparation of Soil Samples for Particle Size Analysis and Determination of Soil Constants

D 422 Test Method for Particle Size Analysis of Soils

D 653 Terminology Relating to Soil, Rock, and Contained Fluids

D 1452 Practice for Soil Investigation and Sampling by Auger Borings

D 1586 Method for Penetration Test and Split-Barrel Sampling of Soils

D 1587 Practice for Thin-Walled Tube Sampling of Soils

D 2113 Practice for Rock Core Drilling and Sampling of Rock for Site Investigation

D 2217 Practice for Wet Preparation of Soil Samples for Particle Size Analysis and Determination of Soil Constants

[1] This practice is under the jurisdiction of ASTM Committee D18 on Soil and Rock and is the direct responsibility of Subcommittee D18.21.05 on Design and Installation of Ground-Water Monitoring Wells.

Current edition approved Jan. 1, 2004. Published March 2004. Originally approved in 1990. Last previous edition approved in 2002 as D 5092 – 02.

[2] For referenced ASTM standards, visit the ASTM website, www.astm.org, or contact ASTM Customer Service at service@astm.org. For *Annual Book of ASTM Standards* volume information, refer to the standard's Document Summary page on the ASTM website.

D 2487 Practice for Classification of Soils for Engineering Purposes (Unified Soil Classification System)
D 2488 Practice for Description and Identification of Soils (Visual-Manual Procedure)
D 3282 Practice for Classification of Soils and Soil Aggregate Mixtures for Highway Construction Purposes
D 3441 Test Method for Deep, Quasi-Static, Cone and Friction Cone Penetration Tests of Soil
D 3550 Practice for Ring Lined Barrel Sampling of Soils
D 4220 Practice for Preserving and Transporting Soil Samples
D 4700 Guide for Soil Sampling from the Vadose Zone
D 4750 Test Method for Determining Subsurface Liquid Levels in a Borehole or Monitoring Well (Observation Well)
D 5079 Practices for Preserving and Transporting Rock Core Samples
D 5088 Practice for Decontamination of Field Equipment Used at Nonradioactive Waste Sites
D 5254 Practice for Minimum Set of Data Elements to Identify a Ground-Water Site
D 5299 Guide for Decommissioning of Ground-Water Wells, Vadose Zone Monitoring Devices, Boreholes, and Other Devices for Environmental Activities
D 5434 Guide for Field Logging of Subsurface Explorations of Soil and Rock
D 5518 Guide for Acquisition of File Aerial Photography and Imagery for Establishing Historic Site Use and Surficial Conditions
D 5521 Guide for Development of Ground-Water Monitoring Wells in Granular Aquifers
D 5608 Practice for Decontamination of Field Equipment Used at Low-Level Radioactive Waste Sites
D 5730 Guide to Site Characterization for Environmental Purposes with Emphasis on Soil, Rock, the Vadose Zone, and Ground Water
D 5753 Guide for Planning and Conducting Borehole Geophysical Logging
D 5777 Guide for Using the Seismic Refraction Method for Subsurface Investigation
D 5781 Guide for Use of Dual-Wall Reverse-Circulation Drilling for Geoenvironmental Exploration and Installation of Subsurface Water-Quality Monitoring Devices
D 5782 Guide for Use of Direct Air-Rotary Drilling for Geoenvironmental Exploration and Installation of Subsurface Water-Quality Monitoring Devices
D 5783 Guide for Use of Direct Rotary Drilling with Water-Based Drilling Fluid for Geoenvironmental Exploration and Installation of Subsurface Water-Quality Monitoring Devices
D 5784 Guide for Use of Hollow Stem Augers for Geoenvironmental Exploration and Installation of Subsurface Water-Quality Monitoring Devices
D 5787 Practice for Monitoring Well Protection
D 5872 Guide for the Use of Casing Advancement Drilling Methods for Geoenvironmental Exploration and Installation of Subsurface Water-Quality Monitoring Devices
D 5875 Guide for the Use of Cable Tool Drilling and Sampling Methods for Geoenvironmental Exploration and Installation of Subsurface Water-Quality Monitoring Devices
D 5876 Guide for the Use of Direct Rotary Wireline Casing Advancement Drilling Methods for Geoenvironmental Exploration and the Installation of Subsurface Water-Quality Monitoring Devices
D 5978 Guide for Maintenance and Rehabilitation of Ground-Water Monitoring Wells
D 5979 Guide for Conceptualization and Characterization of Ground-Water Systems
D 6001 Guide for Direct-Push Water Sampling for Geoenvironmental Investigations
D 6067 Guide for Using the Electronic Cone Penetrometer for Environmental Site Characterization
D 6167 Guide for Conducting Borehole Geophysical Logging
D 6169 Guide to the Selection of Soil and Rock Sampling Devices Used With Drilling Rigs for Environmental Investigations
D 6235 Practice for Expedited Site Characterization of Vadose Zone and Ground-Water Contamination at Hazardous Waste Contaminated Sites
D 6274 Guide for Conducting Borehole Geophysical Logging—Gamma
D 6282 Guide for Direct-Push Soil Sampling for Environmental Site Characterization
D 6286 Guide to the Selection of Drilling Methods for Environmental Site Characterization
D 6429 Guide for Selecting Surface Geophysical Methods
D 6430 Guide for Using the Gravity Method for Subsurface Investigation
D 6431 Guide for Using the Direct Current Resistivity Method for Subsurface Investigation
D 6432 Guide for Using the Surface Ground Penetrating Radar Method for Subsurface Investigation
D 6519 Practice for Sampling of Soil Using the Hydraulically Operated Stationary Piston Sampler
D 6639 Guide for Using the Frequency Domain Electromagnetic Method for Subsurface Investigations
D 6640 Guide for Collection and Handling of Soils Obtained in Core Barrel Samplers for Environmental Investigations
D 6724 Guide for the Installation of Direct-Push Ground-Water Monitoring Wells
D 6725 Practice for the Installation of Prepacked Screen Monitoring Wells in Unconsolidated Aquifers
D 6771 Practice for Low-Flow Purging and Sampling for Wells and Devices Used for Ground-Water Quality Investigations
F 480 Specification for Thermoplastic Well Casing and Couplings Made in Standard Dimension Ratios (SDR), Schedule 40 and Schedule 80

## 3. Terminology

3.1 *Definitions:*

3.1.1 *annular space; annulus*—the space between two concentric strings of casing, or between the casing and the borehole wall. This includes the space(s) between multiple strings of casing in a borehole installed either concentrically or adjacent to one another.

3.1.2 *artifactual turbidity*—particulate matter that is not naturally mobile in the ground-water system and that is produced in some way by the ground-water sampling process. May consist of particles introduced to the subsurface during drilling or well construction, sheared from the target monitoring zone during pumping or bailing the well, or produced by exposure of ground water to atmospheric conditions.

3.1.3 *assessment monitoring*—an investigative monitoring program that is initiated after the presence of a contaminant in ground water has been detected. The objective of this program is to determine the concentration of constituents that have contaminated the ground water and to quantify the rate and extent of migration of these constituents.

3.1.4 *ballast*—materials used to provide stability to a buoyant object (such as casing within a water-filled borehole).

3.1.5 *borehole*—an open or uncased subsurface hole, generally circular in plan view, created by drilling.

3.1.6 *borehole log*—the record of geologic units penetrated, drilling progress, depth, water level, sample recovery, volumes, and types of materials used, and other significant facts regarding the drilling and/or installation of an exploratory borehole or well.

3.1.7 *bridge*—an obstruction within the annulus that may prevent circulation or proper placement of annular fill materials.

3.1.8 *casing*—pipe, finished in sections with either threaded connections or beveled edges to be field welded, which is installed temporarily or permanently either to counteract caving, to advance the borehole, or to isolate the zone being monitored, or any combination of these.

3.1.9 *casing, protective*—a section of larger diameter pipe that is placed over the upper end of a smaller diameter monitoring well riser or casing to provide structural protection to the well, to prevent damage to the well, and to restrict unauthorized access into the well.

3.1.10 *casing, surface*—pipe used to stabilize a borehole near the surface during the drilling of a borehole that may be left in place or removed once drilling is completed.

3.1.11 *caving; sloughing*—the inflow of unconsolidated material into a borehole that occurs when the borehole walls lose their cohesiveness.

3.1.12 *cement*—commonly known as Portland cement. A mixture that consists of calcareous, argillaceous, or other silica-, alumina-, and iron-oxide-bearing materials that is manufactured and formulated to produce various types which are defined in Specification C 150. Portland cement is considered a hydraulic cement because it must be mixed with water to form a cement-water paste that has the ability to harden and develop strength even if cured under water.

3.1.13 *centralizer*—a device that assists in the centering of a casing or riser within a borehole or another casing.

3.1.14 *confining unit*—a body of relatively low hydraulic conductivity formation material stratigraphically adjacent to one or more aquifers. Synonymous with "aquiclude,"" aquitard," and "aquifuge."

3.1.15 *detection monitoring*—a program of monitoring for the express purpose of determining whether or not there has been a contaminant release to ground water.

3.1.16 *d-10*—the diameter of a soil particle (preferably in mm) at which 10 % by weight (dry) of the particles of a particular sample are finer. Synonymous with the effective size or effective grain size.

3.1.17 *d-60*—the diameter of a soil particle (preferably in mm) at which 60 % by weight (dry) of the particles of a particular sample are finer.

3.1.18 *flush joint or flush coupled*—casing or riser with ends threaded such that a consistent inside and outside diameter is maintained across the threaded joints or couplings.

3.1.19 *gravel pack*—common term used to refer to the primary filter pack of a well (see *primary filter pack*).

3.1.20 *grout (monitoring wells)*—a low-permeability material placed in the annulus between the well casing or riser and the borehole wall (in a single-cased monitoring well), or between the riser and casing (in a multi-cased monitoring well), to prevent movement of ground water or surface water within the annular space.

3.1.21 *hydrologic unit*—geologic strata that can be distinguished on the basis of capacity to yield and transmit fluids. Aquifers and confining units are types of hydrologic units. Boundaries of a hydrologic unit may not necessarily correspond either laterally or vertically to lithostratigraphic formations.

3.1.22 *multi-cased well*—a well constructed by using successively smaller diameter casings with depth.

3.1.23 *neat cement*—a mixture of Portland cement (Specification C 150) and water.

3.1.24 *packer (monitoring wells)*—a transient or dedicated device placed in a well that isolates or seals a portion of the well, annulus, or borehole at a specific level.

3.1.25 *piezometer*—a small-diameter well with a very short screen that is used to measure changes in hydraulic head, usually in response to pumping a nearby well. Synonymous with observation well.

3.1.26 *primary filter pack*—a clean silica sand or sand and gravel mixture of selected grain size and gradation that is installed in the annular space between the borehole wall and the well screen, extending an appropriate distance above the screen, for the purpose of retaining and stabilizing the particles from the adjacent formation(s). The term is used in place of *gravel pack*.

3.1.27 *PTFE tape*—joint sealing tape composed of polytetrafluoroethylene.

3.1.28 *riser*—the pipe or well casing extending from the well screen to just above or below the ground surface.

3.1.29 *secondary filter pack*—a clean, uniformly graded sand that is placed in the annulus between the primary filter pack and the overlying seal, or between the seal and overlying grout backfill, or both, to prevent intrusion of the seal or grout, or both, into the primary filter pack.

3.1.30 *sediment sump*—a blank extension of pipe or well casing, closed at the bottom, beneath the well screen used to collect fine-grained material from the filter pack and adjacent formation materials during the process of well development. Synonymous with rat trap or tail pipe.

3.1.31 *single-cased well*—a monitoring well constructed with a riser but without an exterior casing.

3.1.32 *static water level*—the elevation of the top of a column of water in a monitoring well or piezometer that is not influenced by pumping or conditions related to well installation, or hydraulic testing.

3.1.33 *tamper*—a heavy cylindrical metal section of tubing that is operated on a wire rope or cable. It either slips over the riser and fits inside the casing or borehole annulus, or fits between the riser and annulus. It is generally used to tamp annular sealants or filter pack materials into place and to prevent bridging or break bridges that form in the annular space.

3.1.34 *target monitoring zone*—the ground-water flow path from a particular area or facility in which monitoring wells will be screened. The target monitoring zone should be an interval in subsurface materials in which there is a reasonable expectation that a monitoring well will intercept ground water moving beneath an area or facility and any migrating contaminants that may be present.

3.1.35 *tremie pipe*—a small-diameter pipe or tube that is used to transport filter pack materials and annular seal materials from the ground surface into an annular space.

3.1.36 *uniformity coefficient*—the ratio of d-60/d-10, where d-60 and d-10 are particle diameters corresponding to 60 % and 10 % finer on the cumulative particle size curve, respectively.

3.1.37 *uniformly graded*—a quantitative definition of the particle size distribution of a soil that consists of a majority of particles being of approximately the same diameter. A granular material is considered uniformly graded when the uniformity coefficient is less than about five (Test Method D 2487). Comparable to the geologic term *well sorted*.

3.1.38 *vented cap*—a cap with a small hole that is installed on top of the riser.

3.1.39 *weep hole*—a small-diameter hole (usually ¼ in.) drilled into the protective casing above the ground surface that serves to drain out water that may enter the annulus between the riser and the protective casing.

3.1.40 *well completion diagram*—a record that illustrates the details of a well installation.

3.1.41 *well screen*—a device used to retain the primary or natural filter pack; usually a cylindrical pipe with openings of a uniform width, orientation, and spacing.

## 4. Significance and Use

4.1 This practice for the design and installation of ground-water monitoring wells will promote *(1)* efficient and effective site hydrogeological characterization; *(2)* durable and reliable well construction; and *(3)* acquisition of representative ground-water quality samples, ground-water levels, and hydraulic conductivity testing data from monitoring wells. The practices established herein are affected by governmental regulations and by site-specific geological, hydrogeological, climatological, topographical, and subsurface geochemical conditions. To meet these geoenvironmental challenges, this practice promotes the development of a conceptual hydrogeologic model prior to monitoring well design and installation.

4.2 A properly designed and installed ground water monitoring well provides essential information on one or more of the following subjects:

4.2.1 Formation geologic and hydraulic properties;

4.2.2 Potentiometric surface of a particular hydrologic unit(s);

4.2.3 Water quality with respect to various indicator parameters; and

4.2.4 Water chemistry with respect to a contaminant release.

## 5. Site Characterization

5.1 *General*—A thorough knowledge of site-specific geologic, hydrologic and geochemical conditions is necessary to properly apply the monitoring well design and installation procedures contained within this practice. Development of a conceptual site model, that identifies potential flow paths and the target monitoring zone(s), and generates a 3-D picture of contaminant distribution and contaminant movement pathways, is recommended prior to monitoring well design and installation. Development of the conceptual site model is accomplished in two phases -- an initial reconnaissance, after which a preliminary conceptual model is created, and a field investigation, after which a revised conceptual model is formulated. When the hydrogeology of a project area is relatively uncomplicated and well documented in the literature, the initial reconnaissance may provide sufficient information to identify flow paths and the target monitoring zone(s). However, where limited or no background data are available or where the geology is complex, a field investigation will be required to develop the necessary conceptual site model.

5.2 *Initial Reconnaissance of Project Area*—The goal of the initial reconnaissance of the project area is to identify and locate those zones or preferential flow pathways with the greatest potential to transmit fluids from the project area. Identifying these flow pathways is the first step in selecting the target ground-water monitoring zone(s).

5.2.1 *Literature Search*—Every effort should be made to collect and review all applicable field and laboratory data from previous investigations of the project area. Information such as, but not limited to, topographic maps, aerial imagery (see Guide D 5518), site ownership and utilization records, geologic and hydrogeologic maps and reports, mineral resource surveys, water well logs, information from local well drillers, agricultural soil reports, geotechnical engineering reports, and other engineering maps and reports related to the project area should be reviewed to locate relevant site information.

5.2.2 *Field Reconnaissance*—Early in the investigation, the soil and rocks in open cut areas (e.g., roadcuts, streamcuts) in the vicinity of the project should be studied, and various soil and rock profiles noted. Special consideration should be given to soil color and textural changes, landslides, seeps, and springs within or near the project area.

5.2.3 *Preliminary Conceptual Model*—The distribution of the predominant soil and rock units likely to be found during subsurface exploration may be hypothesized at this time in a preliminary conceptual site model using information obtained in the literature search and field reconnaissance. In areas where the geology is relatively uniform, well documented in the literature, and substantiated by the field reconnaissance, further refinement of the conceptual model may not be necessary unless anomalies are discovered in the well drilling stage.

5.3 *Field Investigation*—The goal of the field investigation is to refine the preliminary conceptual site model so that the target monitoring zone(s) is (are) identified prior to monitoring well installation.

5.3.1 *Exploratory Borings and Direct-Push Methods*—Characterization of the flow paths conceptualized in the initial reconnaissance involves defining the porosity (type and amount), hydraulic conductivity, stratigraphy, lithology, gradation and structure of each hydrologic unit encountered beneath the site. These characteristics are defined by conducting an exploratory program which may include drilled soil borings (see Guide D 6286 for selection of drilling methods) and direct-push methods (e.g., cone penetrometers [see Test Method D 3441 or Guide D 6067] or direct-push machines using soil sampling, ground-water sampling and/or electrical conductivity measurement tools [see Guides D 6282 and D 6001]). Exploratory soil borings and direct-push holes should be deep enough to develop the required engineering and hydrogeologic data for determining the preferential flow pathway(s), target monitoring zone(s), or both.

5.3.1.1 *Sampling*—Soil and rock properties should not be predicted wholly on field description or classification, but should be confirmed by laboratory and/or field tests made on samples or in boreholes or wells. Representative soil or rock samples of each material that is significant to the design of the monitoring well system should be obtained and evaluated by a geologist, hydrogeologist, soil scientist or engineer trained and experienced in soil and rock analysis. Soil sample collection should be conducted according to Practice D 1452, Test Method D 1586, Practice D 3550, Practice D 6519 or Practice D 1587, whichever is appropriate given the anticipated characteristics of the soil samples (see Guide D 6169 for selection of soil sampling methods). Rock samples should be collected according to Practice D 2113. Soil samples obtained for evaluation of hydraulic properties should be containerized and identified for shipment to a laboratory. Special measures to preserve either the continuity of the sample or the natural moisture are not usually required. However, soil and rock samples obtained for evaluation of chemical properties often require special field preparation and preservation to prevent significant alteration of the chemical constituents during transportation to a laboratory (see Practice D 6640). Rock samples for evaluation of hydraulic properties are usually obtained using a split-inner-tube core barrel. Evaluation and logging of the core samples is usually done in the field before the core is removed from the core barrel.

5.3.1.2 *Boring Logs*—Care should be taken to prepare and retain a complete boring log and sampling record for each exploratory soil boring or direct-push hole (see Guide D 5434).

NOTE 1—Site investigations conducted for the purpose of generating data for the installation of ground-water monitoring wells can vary greatly due to the availability of reliable site data or the lack thereof. The general procedure would be as follows: *(1)* gather factual data regarding the surficial and subsurface conditions, *(2)* analyze the data, *(3)* develop a conceptual model of the site conditions, *(4)* locate the monitoring wells based on the first three steps. Monitoring wells should only be installed with sufficient understanding of the geologic, and hydrologic and geochemical conditions present at the site. Monitoring wells often serve as part of an overall site investigation for a specific purpose, such as determining the extent of contamination present, or for predicting the effectiveness of aquifer remediation. In these cases, extensive additional geotechnical and hydrogeologic information may be required that would go beyond the Section 5 Site Characterization description.

Boring logs should include the location, geotechnical data (that is, penetration rates or blow counts), and sample description information for each material identified in the borehole either by symbol or word description, or both. Description and identification of soils should be in accordance with Practice D 2488; classification of soils should be in accordance with either Practice D 2487 or Practice D 3282. Identification of rock material should be based on Nomenclature C 294 or by an appropriate geologic classification system. Observations of seepage, free water, and water levels should also be noted. The boring logs should be accompanied by a report that includes a description of the area investigated; a map illustrating the vertical and horizontal location (with reference to either North American Vertical Datum of 1988 [NAVD 88] or to a standardized survey grid) of each exploratory soil boring or test pit, or both; and color photographs of rock cores, soil samples, and exposed strata labeled with a date and identification.

5.3.2 *Geophysical Exploration*—Geophysical surveys may be used to supplement soil boring and outcrop observation data and to aid in interpretation between soil borings. Appropriate surface and borehole geophysical methods for meeting site-specific project objectives can be selected by consulting Guides D 6429 and D 5753 respectively. Surface geophysical methods such as seismic (Guide D 5777), electrical-resistivity (Guide D 6431), ground-penetrating radar (Guide D 6432), gravity (Guide D 6430) and electromagnetic conductance surveys (Guide D 6639) can be particularly valuable when distinct differences in the properties of contiguous subsurface materials are indicated. Borehole methods such as resistivity, gamma, gamma-gamma, neutron, and caliper logs (see Guide D 6167) can be useful to confirm specific subsurface geologic conditions. Gamma logs (Guide D 6274) are particularly useful in existing cased wells.

5.3.3 *Ground-Water Flow Direction*—Ground-water flow direction is generally determined by measuring the vertical and horizontal hydraulic gradient within each conceptualized flow pathway. However, because water will flow along the pathways of least resistance (within the highest hydraulic conductivity formation materials at the site), actual flow direction may be oblique to the hydraulic gradient (within buried stream channels or glacial valleys, for example). Flow direction is determined by first installing piezometers in the exploratory soil borings that penetrate the zone(s) of interest at the site. The depth and location of the piezometers will depend upon anticipated hydraulic connections between conceptualized flow pathways and their respective lateral direction of flow. Following careful evaluation, it may be possible to utilize existing private or public wells to obtain water-level data. The construction integrity of such wells should be verified to ensure that the water levels obtained from the wells are representative only of the zone(s) of interest. Following water-level data acquisition, a potentiometric surface map should be prepared. Flow pathways are ordinarily determined to be at right angles, or nearly so, to the equipotential lines, though consideration of complex geology can result in more complex interpretations of flow

5.4 *Completing the Conceptual Model*—A series of geologic and hydrogeologic cross sections should be developed to refine the conceptual model. This is accomplished by first plotting logs of soil and rock observed in the exploratory soil borings or test pits, and interpreting between these logs using the geologic and engineering interrelationships between other soil and rock data observed in the initial reconnaissance or with geophysical techniques. Extrapolation of data into adjacent areas should be done only where geologically uniform subsurface conditions are known to exist. The next step is to integrate the geologic profile data with the potentiometric data for both vertical and horizontal hydraulic gradients. Plan view and cross-sectional flow nets should be constructed. Following the analysis of these data, conclusions can be made as to which flow pathway(s) is (are) the appropriate target monitoring zone(s).

NOTE 2—UUse of ground-water monitoring wells is difficult and may not be a reliable technology in fine-grained, low hydraulic conductivity formation materials with primary porosity because of *(1)* the disproportionate influence that microstratigraphy has on ground-water flow in fine-grained strata; *(2)* the proportionally higher vertical flow component in low hydraulic conductivity strata; and *(3)* the presence of indigenous metallic and inorganic constituents in the matrix that make water-quality data evaluation difficult.

## 6. Monitoring Well Construction Materials

6.1 *General*—The materials that are used in the construction of a monitoring well that come in contact with water samples should not alter the chemical quality of the sample for the constituents being examined. The riser, well screen, and annular seal installation equipment should be cleaned immediately prior to well installation (see either Practice D 5088 or D 5608) or certified clean from the manufacturer and delivered to the site in a protective wrapping. Samples of the riser and screen material, cleaning water, filter pack, annular seal, bentonite, and mixed grout should be retained to serve as quality control until the completion of at least one round of ground- water quality sampling and analysis has been completed.

6.2 *Water*—Water used in the drilling process, to prepare grout mixtures and to decontaminate the well screen, riser, and annular sealant injection equipment, should be obtained from a source of known chemistry that does not contain constituents that could compromise the integrity of the well installation.

6.3 *Primary Filter Pack*:

6.3.1 *General*—The purposes of the primary filter pack are to act as a filter that retains formation material while allowing ground water to enter the well, and to stabilize the formation to keep it from collapsing on the well. The design of the primary filter pack is based on the grain-size distribution of the formation material (as determined by sieve analysis—see Test Method D 422) to be retained. The grain size distribution of the primary filter pack must be fine enough to retain the formation, but coarse enough to allow for unrestricted movement of ground water into and through the monitoring well. The design of the well screen (see 6.4.3) must be done in concert with the design of the filter pack. After development, a monitoring well with a correctly designed and installed filter pack and screen combination should produce samples free of artifactual turbidity.

6.3.2 *Materials*—The primary filter pack should consist of an inert granular material (generally ranging from gravel to very fine sand, depending on formation grain size distribution) of selected grain size and gradation that is installed in the annulus between the well screen and the borehole wall. Washed and screened silica sands and gravels, with less than 5 % non-siliceous materials, should be specified.

6.3.3 *Design*—The design theory of filter pack gradation is based on mechanical retention of formation materials.

6.3.3.1 1 For formation materials that are relatively coarse-grained (i.e., fine, medium and coarse sands and gravels), the grain size distribution of the primary filter pack is determined by calculating the d-30 (30 % finer) size, the d-60 (60 % finer) size, and the d-10 (10 % finer) size of the filter pack. The first point on the filter pack grain-size distribution curve is the d-30 size. The primary filter pack is usually selected to have a d-30 grain size that is about 4 to 6 times greater than the d-30 grain size of the formation material being retained (see Fig. 1). A multiplication factor of 4 is used if the formation material is relatively fine-grained and well sorted or uniform (small range in grain sizes); a multiplication factor of 6 is used if the formation is relatively coarse grained and poorly sorted or non-uniform (large range in grain sizes). Thus, 70 % of the filter pack will have a grain size that is 4 to 6 times larger than the d-30 size of the formation materials. This ensures that the filter pack is coarser (with a higher hydraulic conductivity) than the formation material, and allows for unrestricted ground-water flow from the formation into the monitoring well.

The next 2 points on the filter pack grain-size distribution curve are the d-60 and d-10 grain sizes. These are chosen so that the ratio between the two grain sizes (the uniformity coefficient) is less than 2.5. This ensures that the filter pack has a small range in grain sizes and is uniform (see technical Note 5). The d-60 and d-10 grain sizes of the filter pack are calculated by a trial and error method using grain sizes that are close to the d-30 size of the filter pack. After the d-30, d-60 and d-10 sizes of the filter pack are determined, a smooth curve is drawn through these points. The final step in filter pack design is to specify the limits of the grain size envelope, which defines the permissible range in grain sizes for the filter pack. The permissible range on either side of the grain size curve is 8 %. The boundaries of the grain size envelope are drawn on either side of the filter pack grain-size distribution curve, and filter pack design is complete. A filter medium having a grain-size distribution as close as possible to this curve is then obtained from a local sand supplier.

6.3.3.2 In formation materials that are predominantly fine-grained (finer than fine to very fine sands), soil piping can occur when a hydraulic gradient exists between the formation and the well (as would be the case during well development and sampling). To prevent soil piping in these materials, the following criteria are used for designing granular filter packs:

$$\frac{\text{d-15 of filter}}{\text{d-85 of formation}} \leq 4 \text{ to } 5 \quad \text{and} \quad \frac{\text{d-15 of filter}}{\text{d-15 of formation}} \geq 4 \text{ to } 5$$

The left half of this equation is the fundamental criterion for the prevention of soil piping through a granular filter, while the right half of the equation is the hydraulic conductivity criterion. This latter criterion serves the same purpose as multiplying the d-30 grain size of the formation by a factor of between 4 and 6 for coarser formation materials. Filter pack materials suitable for retaining formation materials in formations that are predominantly fine-grained are themselves, by necessity, relatively fine-grained (e.g., fine to very fine sands), presenting several problems for well designers and installers. First, well screen slot sizes suitable for retaining such fine-grained filter pack materials are not widely available (the smallest commercially available slotted well casing is 0.006 in. [6 slot]; the smallest commercially available continuous-slot wire-wound screen is 0.004 in. [4 slot]). Second, the finest filter pack material practical for conventional (tremie tube) installation is a 40 by 70 (0.008 by 0.018 in.) sand, which can be used with a well screen slot as small as 0.008-in. (8 slot). Finer grained filter pack materials cannot be placed practically by either tremie tubes or pouring down the annular space or down augers. Thus, the best method for ensuring proper installation of filter packs in predominantly fine-grained formation materials is to use pre-packed or sleeved screens, which are described in detail in Practice D 6725. A 50 by 100 (0.011 by 0.006 in.) filter-pack sand can be used with a 0.006-in. slot size pre-packed or sleeved screen, and a 60 by 120 (0.0097 by 0.0045 in.) filter-pack sand can be used with a 0.004-in. (4 slot) slot size pre-packed or sleeved screen. Filter packs that are finer than these (e.g., sands as fine as 100 by 120 [0.006 by 0.0045 in.], or silica flour as fine as 200 mesh [0.003 in.]) can only be installed within stainless steel mesh sleeves that can be placed over pipe-based screens. While these sleeves, or the space between internal and external screens in a pre-packed well screen may be as thin as 1/2-in. (1.27 cm), the basis for mechanical retention dictates that a filter-pack thickness of only two or three grain diameters is needed to contain and control formation materials. Laboratory tests have demonstrated that a properly sized filter pack material with a thickness of less than 1/2-in. (1.27 cm) successfully retains formation particles regardless of the velocity of water passing through the filter pack [3].

[3] (1) Driscoll, F.G., 1986, Groundwater and Wells, Johnson Division, St. Paul, MN, pg.443

6.3.3.3 The limit of mechanical filtration for monitoring wells is defined by the finest filter pack material that can be practically installed via a pre-packed or sleeved screen—silica flour with a grain size of 0.003 in. (200 mesh), encased within a very fine mesh screen of stainless steel or other suitable material. This fine a filter pack material will retain formation material as fine as silt, but not clay. Formations with a small fraction of clay (up to about 20 %) can be successfully monitored, as long as the wells installed in these formations are properly developed (see Guide D 5521). For mechanical filtration to be effective in formations with more than 50 % fines, the filter pack design would have to include silt-sized particles in the filter pack in order to meet the design criteria, which is impractical, as placement would be impossible and screen mesh fine enough to retain the material is not commercially available. Therefore, formations with more than 50 % passing a #200 sieve, and having more than 20 % clay-sized material, should not be monitored using conventional well designs. Alternative monitoring technologies should be used in these formations.

NOTE 3—When installing a monitoring well in solution-channeled limestone or highly fractured bedrock, the borehole configuration of void spaces within the formation surrounding the borehole is often unknown. Therefore, the installation of a filter pack becomes difficult and may not be possible.

NOTE 4—This practice presents a design for monitoring wells that will be effective in the majority of formations. Applicable state guidance may differ from the designs contained in this practice.

NOTE 5—Because the well screen slots have uniform openings, the filter pack should be composed of particles that are as uniform in size as is practical. Ideally, the uniformity coefficient (the quotient of the 60 % passing, D-60 size divided by the 10 % passing D-10 size [effective size]) of the filter pack should be 1.0 (that is, the D-60 % and the D-10 % sizes should be identical). However, a more practical and consistently achievable uniformity coefficient for all ranges of filter pack sizes is 2.5. This value of 2.5 should represent a maximum value, not an ideal.

NOTE 6—Although not recommended as standard practice, often a project requires drilling and installing the well in one phase of work. Therefore, the filter pack materials must be ordered and delivered to the drill site before soil samples can be collected. In these cases, the suggested well screen slot size and filter pack material combinations are presented in Table 1.

NOTE 7—Silica flour can alter water chemistry, particularly for transuranics, and its use should be evaluated against the monitoring program analytes

6.4 *Well Screen*:

6.4.1 *General*—The purposes of the well screen are to provide designed openings for ground-water flow through the well, and to prevent migration of filter pack and formation

**TABLE 1 Recommended (Achievable) Filter Pack Characteristics for Common Screen Slot Sizes**

| Size of Screen Opening, mm (in.) | Slot No. | Sand Pack Mesh Size Name(s) | 1 % Passing Size (D-1), mm | Effective Size, (D-10), mm | 30 % Passing Size (D-30), mm | Range of Uniformity Coefficient | Roundness (Powers Scale) |
|---|---|---|---|---|---|---|---|
| 0.125 (0.005) | 5[A] | 100 | 0.09 to 0.12 | 0.14 to 0.17 | 0.17 to 0.21 | 1.3 to 2.0 | 2 to 5 |
| 0.25 (0.010) | 10 | 20 to 40 | 0.25 to 0.35 | 0.4 to 0.5 | 0.5 to 0.6 | 1.1 to 1.6 | 3 to 5 |
| 0.50 (0.020) | 20 | 10 to 20 | 0.7 to 0.9 | 1.0 to 1.2 | 1.2 to 1.5 | 1.1 to 1.6 | 3 to 6 |
| 0.75 (0.030) | 30 | 10 to 20 | 0.7 to 0.9 | 1.0 to 1.2 | 1.2 to 1.5 | 1.1 to 1.6 | 3 to 6 |
| 1.0 (0.040) | 40 | 8 to 12 | 1.2 to 1.4 | 1.6 to 1.8 | 1.7 to 2.0 | 1.1 to 1.6 | 4 to 6 |
| 1.5 (0.060) | 60 | 6 to 9 | 1.5 to 1.8 | 2.3 to 2.8 | 2.5 to 3.0 | 1.1 to 1.7 | 4 to 6 |
| 2.0 (0.080) | 80 | 4 to 8 | 2.0 to 2.4 | 2.4 to 3.0 | 2.6 to 3.1 | 1.1 to 1.7 | 4 to 6 |

[A] A 5-slot (0.152-mm) opening is not currently available in slotted PVC but is available in Vee wire PVC and Stainless; 6-slot opening may be substituted in these cases.

material into the well. The well screen design is based on either the grain-size distribution of the formation (in the case of a well with a naturally developed filter pack), or the grain-size distribution of the primary filter pack material (in the case of a filter-packed well). The screen openings must be small enough to retain most if not all of the formation or filter-pack materials, yet large enough to maintain ground-water flow velocities, from the well screen/filter pack interface back to the natural formation materials, of less than 0.10 ft/s (0.03 m/s). If well screen entrance velocities exceed 0.10 ft/s (0.03 m/s), turbulent flow conditions can occur, resulting in mobilization of sediment from the formation and reductions in well efficiency.

6.4.2 *Materials*—TThe well screen should be new, machine-slotted casing or continuous wrapped wire-wound screen composed of materials compatible with the monitoring environment, as determined by the site characterization program. The screen should be plugged at the bottom (unless a sediment sump is used), and the plug should generally be of the same material as the well screen. This assembly must have the capability to withstand well installation and development stresses without becoming dislodged or damaged. The length of the well screen open area should reflect the thickness of the target monitoring zone. Immediately prior to installation, the well screen should be cleaned (see either Practice D 5088 or Practice D 5608) with water from a source of known chemistry, if it is not certified clean by the manufacturer, and delivered, and maintained in a clean environment at the site.

NOTE 8—Well screens are most commonly composed of PVC or stainless steel. Stainless steel may be specified based on knowledge of the occurrence of microbially influenced corrosion in formations (specifically reducing or acid-producing conditions).

6.4.3 *Diameter*—TThe minimum nominal internal diameter of the well screen should be chosen based on factors specific to the particular application (such as the outside diameter of the purging and sampling device(s) to be used in the well). Well screens as small as 1/2-in. (1.27 cm) nominal diameter are available for use in monitoring well applications.

6.4.4 *Design*—The design of the well screen should be determined based on the grain size analysis (per Test Method D 422) of the interval to be monitored and the gradation of the primary filter pack material. In granular, non-cohesive formation materials that will fall in easily around the screen, filter packs can be developed from the native formation materials—filter pack materials foreign to the formation are not necessary. In these cases of naturally developed filter packs, the slot size of the well screen is determined using the grain size of the materials in the surrounding formation. The well screen slot size selected for this type of well completion should retain at least 70 % of formation materials—the finest 30 % of formation materials will be brought into the well during development, and the objectives of filter packing (to increase hydraulic conductivity immediately surrounding the well screen, and to promote easy flow of ground water into and through the screen) will be met. In wells in which a filter pack material of a selected grain size distribution is introduced from the surface, the screen slot size selected should retain at least 90 %, and preferably 99 %, of the primary filter pack materials. The method for determining the primary filter pack design is described in 6.3.3.

6.4.5 *Prepacked or Sleeved Well Screens*—An alternative to designing and installing filter pack and well screens separately is to use a pre-packed or sleeved screen assembly. A pre-packed well screen consists of an internal well screen, an external screen or filter medium support structure, and the filter medium contained between the screens, which together comprise an integrated structure. The internal and external screens are constructed of materials compatible with the monitored environment, and are usually of a common slot size specified by the well designer to retain the filter pack material. The filter pack is normally an inert (e.g., siliceous) granular material that has a grain-size distribution chosen to retain formation materials. A sleeved screen consists of a slotted pipe base over which a sleeve of stainless steel mesh filled with selected filter media is installed. Pre-packed or sleeved screens may be used for any formation conditions, but they are most often used where heaving, running or blowing sands make accurate placement of conventional well screens and filter packs difficult, or where predominantly fine-grained formation materials are encountered. In the latter case, using pre-packed or sleeved screens is the only practical means of ensuring that filter pack materials of the selected grain-size distribution (generally fine to very fine sands) are installed to completely surround the screen.

NOTE 9—The practice of using a single well screen/filter pack combination (e.g., 0.010 in. [0.254 mm]) well screen slot size with a 20/40 sand) for all wells, regardless of formation grain-size distribution, will result in siltation of the well and significant turbidity in samples when applied to formations finer than the recommended design. It will also result in the loss of filter pack, possible collapse of the screen, and invasion of overlying well construction materials (e.g., secondary filter pack, annular seal materials, grout) when applied to formations coarser than the recommended design. For these reasons, the universal application of a single well screen/filter pack combination to all formations is not recommended, and should be avoided.

6.5 *Riser*:

6.5.1 *Materials*—TThe riser should be new pipe composed of materials that will not alter the quality of water samples for the constituents of concern and that will stand up to long-term exposure to the monitoring environment, including potential contaminants. The riser should have adequate wall thickness and coupling strength to withstand the stresses imposed on it during well installation and development. Each section of riser should be cleaned (see either Practice D 5088 or Practice D 5608) using water from a source of known chemistry immediately prior to installation.

NOTE 10—Risers are generally constructed of PVC, galvanized steel or stainless steel.

6.5.2 *Diameter*—The minimum nominal internal diameter of the riser should be chosen based on the particular application. Risers as small as ½-in. (1.25-cm) in diameter are available for applications in monitoring wells.

6.5.3 *Joints (Couplings)*—Threaded joints are recommended. Glued or solvent-welded joints of any type are not recommended because glues and solvents may alter the chemistry of water samples. Because square profile flush joint threads (Specification F 480) are designed to be accompanied by O-ring seals at the joints, they do not require PTFE taping. However, tapered threaded joints should be PTFE taped to prevent leakage of water into the riser.

6.6 *Casing*—Where conditions warrant, the use of permanent casing installed to prevent communication between water-bearing zones is encouraged. The following subsections address both temporary and permanent casings.

6.6.1 *Materials*—The material type and minimum wall thickness of the casing should be adequate to withstand the forces of installation. All casing that is to remain as a permanent part of the installation (that is, in multi-cased wells) should be new and cleaned to be free of interior and exterior protective coatings.

NOTE 11—The exterior casing (temporary or permanent multi-cased) is generally composed of steel, although other appropriate materials may be used.

6.6.2 *Diameter*—Several different casing sizes may be required depending on the geologic formations penetrated. The diameter of the borehole and the well casing for conventionally filter packed wells should be selected so that a minimum annular space of 2 in. (5 cm) is maintained between the inside diameter of the casing and outside diameter of the riser to provide working space for a tremie pipe. For naturally developed wells and pre-packed or sleeved screen completions, this annular space requirement need not be met. In addition, the diameter of the casings in multi-cased wells should be selected so that a minimum annular space of 2 in. (5 cm) is maintained between the casing and the borehole (that is, a 2-in. [5 cm] diameter screen will require first setting a 6-in. [15.2 cm] diameter casing in a 10-in. [25.4 cm] diameter boring).

NOTE 12—Under difficult drilling conditions (collapsing soils, rock, or cobbles), it may be necessary to advance temporary casing. Under these conditions, a smaller annular space may be maintained.

6.6.3 *Joints (Couplings)*—The ends of each casing section should be either flush-threaded or beveled for welding.

6.7 *Sediment Sump*—A sediment sump, a length of blank pipe, generally of the same diameter and made of the same material as the riser and well screen -- may be affixed to the bottom of the screen, and capped with a bottom plug, to collect fine-grained material brought into the well by the process of well development. A drainage hole may be drilled in the bottom of the sump to prevent the sump from retaining water in the event that the water level outside the well falls below the bottom of the well screen. Because the sediment that collects in the sump may harbor geochemistry-altering microflora and reactive metal oxides, this sediment must be removed periodically to minimize the potential for sample chemical alteration.

6.8 *Protective Casing*:

6.8.1 *Materials*—Protective casings may be made of aluminum, mild steel, galvanized steel, stainless steel, cast iron, or structural plastic pipe. The protective casing should have a lid capable of being locked shut by a locking device or mechanism.

6.8.2 *Diameter*—The inside dimensions of the protective casing should be a minimum of 2 in. (5 cm) and preferably 4 in. (10 cm) larger than the nominal diameter of the riser to facilitate the installation and operation of sampling equipment.

6.9 *Annular Sealants*—TThe materials used to seal the annulus may be prepared as a slurry or used un-mixed in a dry pellet, granular, or chip form. Sealants should be selected to be compatible with ambient geologic, hydrogeologic, geochemical and climatic conditions and any man-induced conditions (e.g., subsurface contamination) anticipated during the life of the well.

6.9.1 *Bentonite*—Bentonite should be powdered, granular, pelletized, or chipped sodium montmorillonite from a commercial source, free of impurities that may adversely impact the water quality in the well. Pellets consist of roughly spherical units of moistened, compressed bentonite powder. Chips are large, irregularly shaped, and coarse granular units of bentonite free of additives. The diameter of pellets or chips selected for monitoring well construction should be less than one fifth the width of the annular space into which they are placed to reduce the potential for bridging. Granules consist of coarse to fine particles of unaltered bentonite, typically smaller than 0.2 in. (5.0 mm). It is recommended that the water chemistry of the formation in which the bentonite is intended for installation be evaluated to ensure that it is suitable to hydrate the bentonite. Some water-quality conditions (e.g., high chloride content, high concentrations of certain organic solvents or petroleum hydrocarbons) may inhibit the hydration of bentonite and result in an ineffective seal.

6.9.2 *Cement*—Each type of cement has slightly different characteristics that may be appropriate under various physical and chemical conditions. Cement should be one of the five Portland cement types that are specified in Specification C 150. The use of quick-setting cements containing additives is not recommended for use in monitoring well installation. Additives may leach from the cement and influence the chemistry of water samples collected from the monitoring well.

6.9.3 *Grout*—The grout backfill that is placed above the bentonite annular seal and secondary filters (see Fig. 1) is ordinarily a thick liquid slurry consisting of either a bentonite (powder or granules, or both) base and water, or a Portland cement base and water. Often, bentonite-based grouts are used when it is desired that the grout remain workable for extended periods of time during well construction or flexible (that is, to accommodate freeze-thaw cycles) during the life of the well. Cement-based grouts are often used when filling cracks in the surrounding geologic material, adherence to rock units, or a rigid setting is desired.

6.9.3.1 *Mixing*—The mixing (and placing) of a grout backfill should be performed with precisely recorded weights and volumes of materials, and according to procedures stipulated by the manufacturer that often include the order of component mixing. The grout should be thoroughly mixed with a paddle-type mechanical mixer or by recirculating the mix through a pump until all lumps are disintegrated. Lumpy grout should not be used in the construction of a monitoring well to prevent bridging within the tremie pipe.

NOTE 13—Lumps do not include lost circulation materials that may be added to the grout if excessive grout losses occur.

6.9.3.2 *Typical Bentonite-Based Grout*—When a bentonite-based grout is used, bentonite, usually unaltered, should be placed in the water through a venturi device. A typical

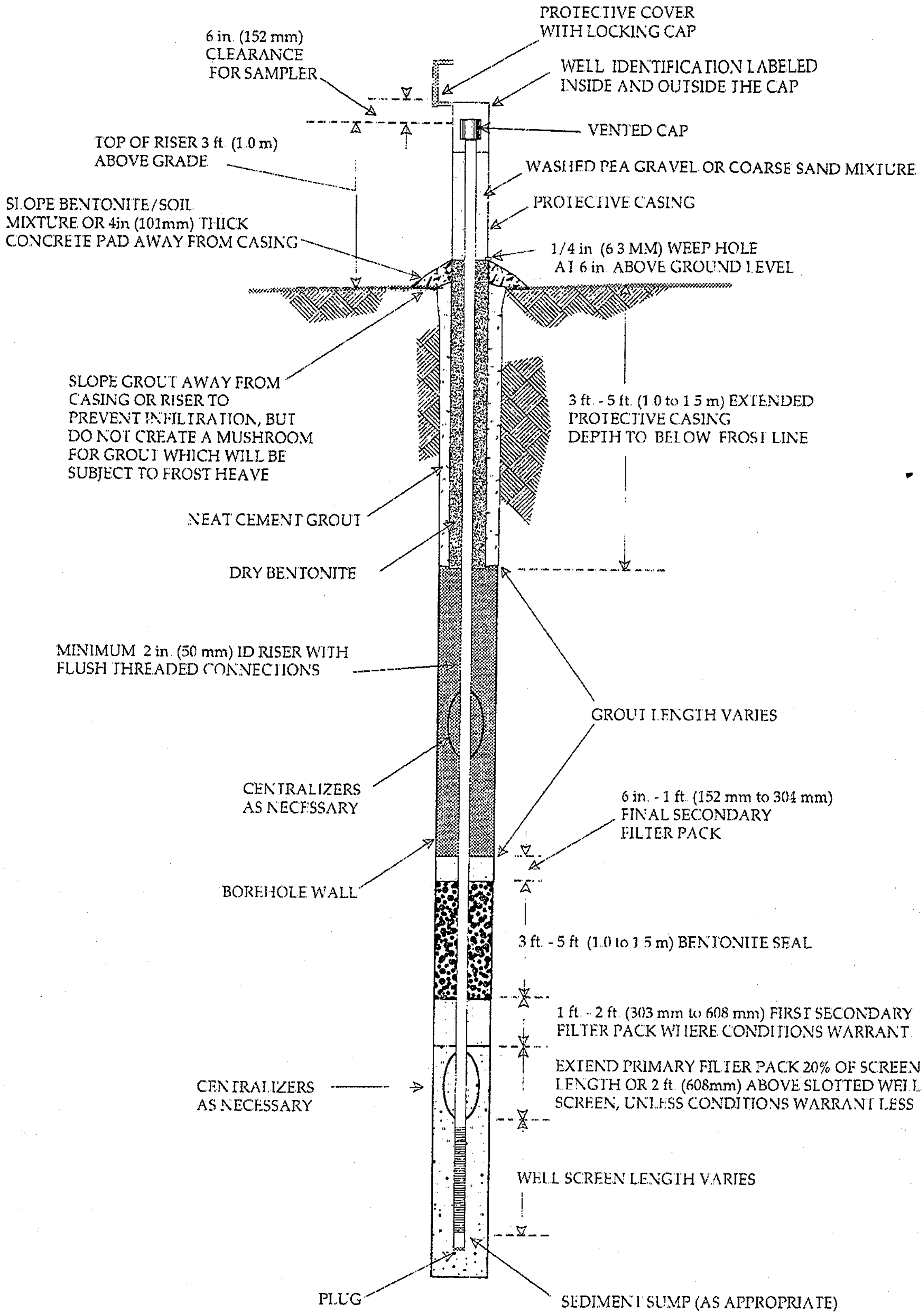



**FIG. 1 Monitoring Well Design—Single-Cased Well**

unbeneficiated bentonite-based grout consists of about 1 to 1.25 lb (0.57 kg) of unaltered bentonite to each 1 gal (3.8 L) of water. 100 % bentonite grouts should not be used for monitoring well annular sealants in the vadose zone of arid regions because of the possibility that they may desiccate. This could result in migration of water into the screened portion of the well from zones above the target monitoring zone.

NOTE 14—High solids bentonite grouts (minimum 20 % by weight with water) and other bentonite-based grouts may contain granular bentonite to increase the solids content and other components added under manufacturer's directions to either stiffen or retard stiffening of the mix. All additives to grouts should be evaluated for their effects on subsequent water samples.

6.9.3.3 *Typical Cement-Based Grout*—A typical cement-based grout consists of about 6 gal. (23 L) of water per 94-lb. (43-kg) bag of Type I Portland cement. Though not recommended because of the chemical incompatability of bentonite with cement (2, 3), from 3 to 8 % (by dry weight) of unaltered bentonite powder is often added after the initial mixing of cement and water to retard shrinkage and provide plasticity..

6.10 *Secondary Filter Packs*:

6.10.1 *Materials*—A secondary filter pack is a layer of material placed in the annulus between the primary filter pack and the bentonite seal, and/or between the bentonite seal and the grout backfill (see Fig. 1 and Fig. 2).

6.10.2 *Gradation*—The secondary filter pack should be uniformly graded fine sand with 100 % by weight passing the #30 U.S. Standard sieve, and less than 2 % by weight passing the #200 U.S. Standard sieve.

6.11 *Annular Seal and Filter Pack Installation Equipment*—The equipment used to install the annular seals and filter pack materials should be cleaned (if appropriate for the selected material) using water from a source of known quality prior to use. This procedure is performed to prevent the introduction of materials that may ultimately alter water quality samples.

## 7. Drilling Methods

7.1 The type of equipment required to create a stable, open, vertical borehole for installation of a monitoring well depends upon the site geology, hydrology, and the intended use of the data. Engineering and geological judgment and some knowledge of subsurface geological conditions at the site is required for the selection of the appropriate drilling method(s) utilized for drilling the exploratory soil borings and monitoring wells (see Guide D 6286). Appropriate drilling methods for investigating and installing monitoring wells at a site may include any one or a combination of several of the following methods: hollow-stem auger (Guide D 5784); direct (mud) rotary (Guide D 5783); direct air-rotary (Guide D 5782); direct rotary wireline casing advancement (Guide D 5876); dual-wall reverse-circulation rotary (Guide D 5781); cable-tool (Guide D 5875); or various casing advancement methods (Guide D 5872). Whenever feasible, it is advisable to utilize drilling procedures that do not require the introduction of water or drilling fluids into the borehole, and that optimize cuttings control at ground surface. Where the use of water or drilling fluid is unavoidable, the selected fluid should have as little impact as possible on the water samples for the constituents of interest. The chemistry of the fluid to be used should be evaluated to determine the potential for water quality sample alteration. In addition, care should be taken to remove as much drilling fluid as possible from the well and the surrounding formation during the well development process. It is recommended that if an air compressor is used, it should be equipped with an oil air filter or oil trap to minimize the potential for chemical alteration of ground-water samples collected after the well is installed. 8. Monitoring Well Installation

## 8. Monitoring Well Installation

8.1 *Stable Borehole*—A stable borehole must be constructed prior to attempting the installation of monitoring well screen and riser. Steps must be taken to stabilize the borehole before attempting installation if the borehole tends to cave or blow in, or both. Boreholes that are not straight or are partially obstructed should be corrected prior to attempting the installation procedures described herein.

8.2 *Assembly of Well Screen and Riser*:

8.2.1 *Handling*—TThe well screen, sediment sump, bottom plug and riser should be either certified clean from the manufacturer or steam-cleaned or high-pressure hot-water washed (whichever is appropriate for the selected material) using water from a source of known chemistry immediately prior to assembly. Personnel should take precautions to assure that grease, oil, or other contaminants that may ultimately alter the water sample do not contact any portion of the well screen and riser assembly. As one precaution, for example, personnel should wear a clean pair of cotton, nitrile or powder-free PVC (or equivalent) gloves while handling the assembly..

8.2.2 *Riser Joints (Couplings)*—Flush joint risers with square profile (Specification F 480) threads do not require PTFE taping to achieve a water tight seal; these joints should not be taped. O-rings made of a material of known chemistry, selected on the basis of compatibility with contaminants of concern and prevailing environmental conditions, should be used to assure a tight seal of flush-joint couplings. Couplings are often tightened by hand; however, if necessary, steam-cleaned or high-pressure water-cleaned wrenches may be utilized. Precautions should be taken to prevent damage to the threaded joints during installation, as such damage may promote leakage past the threads.

8.3 *Setting the Well Screen and Riser Assembly*—When the well screen and riser assembly is lowered to the predetermined level in the borehole and held in position, the assembly may require ballast to counteract the tendency to float in the borehole. Ballasting may be accomplished by filling the riser with water from a source of known and acceptable chemistry or, preferably, using water that was previously removed from the borehole. Alternatively, the riser may be slowly pushed into the fluid in the borehole with the aid of hydraulic rams on the drill rig and held in place as additional sections of riser are added to the column. Care must be taken to secure the riser assembly so that personnel safety is assured during the installation. The assembly must be installed straight and plumb, with centralizers installed at appropriate locations (typically every 20 to 30 ft [6 to 9 m]). Difficulty in maintaining a straight installation may be encountered where the weight of the well screen and riser assembly is significantly less than the buoyant force of the fluid in the borehole. The riser should extend above grade and be capped temporarily to deter entrance of foreign materials during final completion.

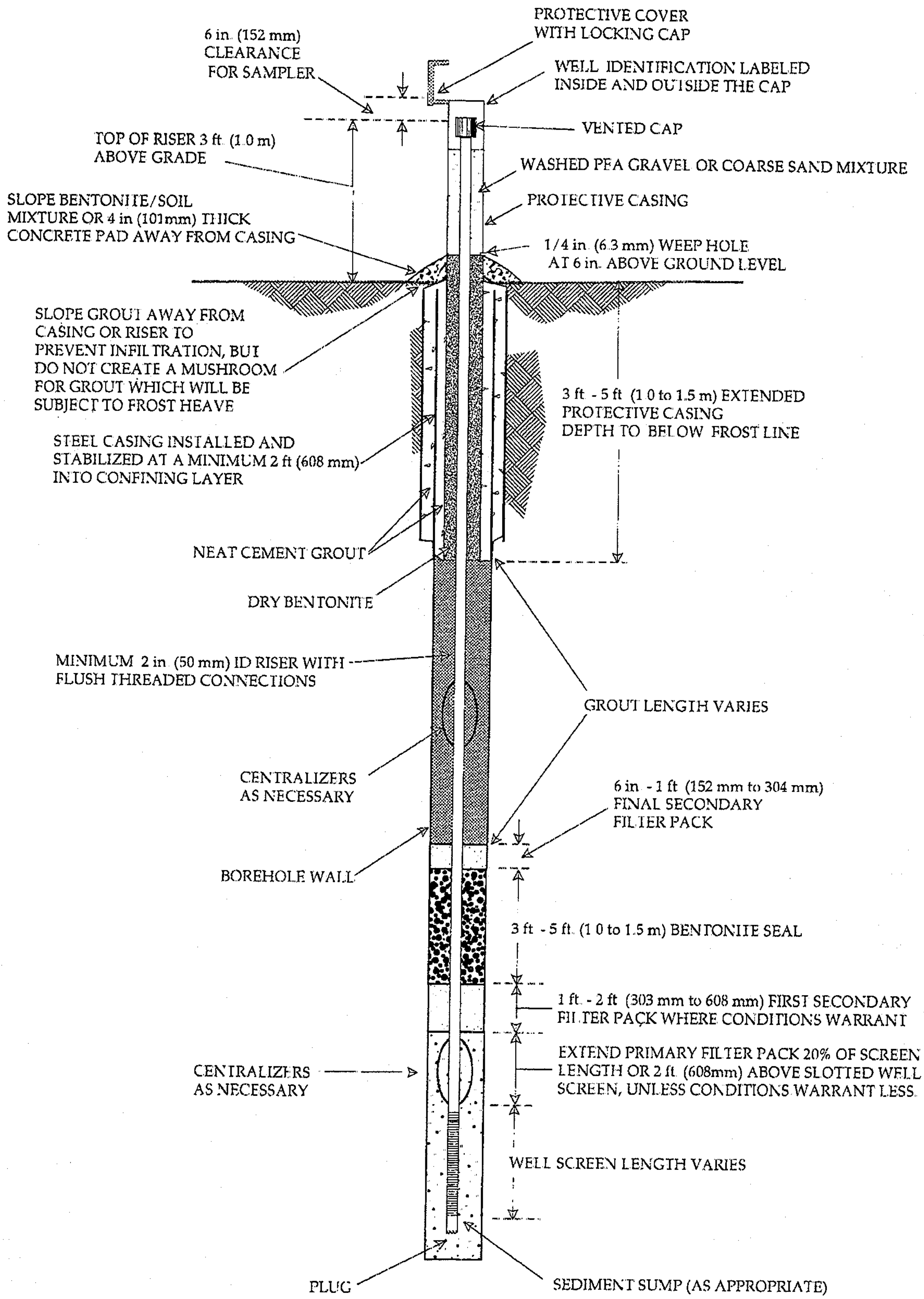



**FIG. 2 Monitoring Well Design—Multi–Cased Well**

8.4 *Installation of the Primary Filter Pack*:

8.4.1 *Volume of Filter Pack*—TThe volume of filter pack required to fill the annular space between the well screen and borehole should be calculated, measured, and recorded on the well completion diagram during installation. To be effective, the filter pack should extend above the screen for a distance of about 20 % of the length of the well screen but not less than 2 ft. (0.6 m) (see Figs. 1 and 2). Where there is hydraulic connection between the zone to be monitored and the overlying strata, this upward extension should be gauged to prevent seepage from overlying hydrologic units into the filter pack. Seepage from other units may alter hydraulic head measurements or the chemistry of water samples collected from the well.

8.4.2 *Placement of Primary Filter Pack*—Placement of the well screen is preceded by placing no less than 2 % and no more than 10 % of the primary filter pack into the bottom of the borehole using a decontaminated, flush threaded, 1-in. (25-mm) minimum internal diameter tremie pipe. Alternatively, the filter pack may be added directly between the riser pipe and the auger or drive/temporary casing and the top of the filter pack located using a tamper or a weighted line. The well screen and riser assembly is then centered in the borehole. This can be done using one or more centralizer(s) or alternative centering devices located not more than 10 ft (3 m) above the bottom of the well screen (see Figs. 1 and 2). Centralizers should not be located in the well screen. The remaining primary filter pack is then placed in increments as the tremie is gradually raised or as the auger or drive/temporary casing is removed from the borehole. As primary filter pack material is poured into the tremie pipe, water from a source of known and acceptable chemistry may be added to help deliver the filter pack to the intended interval in the borehole. The tremie pipe or a weighed line can be used to measure the top of the primary filter pack as work progresses. If bridging of the primary filter pack material occurs, the bridged material should be broken mechanically prior to proceeding with the addition of more filter pack material. The elevation (or depth below ground surface), volume, and gradation of primary filter pack should be recorded on the well completion diagram (see Fig. 2 for an example).

8.4.3 *Withdrawal of the Temporary Casing/Augers*—If used, the drive/temporary casing or hollow stem auger is withdrawn, usually in stipulated increments. Care should be taken to avoid lifting the riser with the withdrawal of the temporary casing/augers. To limit borehole collapse in stable formations, the temporary casing or hollow stem auger is usually withdrawn until the lower-most point on the temporary casing or hollow stem auger is at least 2 ft (0.6 m), but no more than 5 ft (1.5 m) above the filter pack for unconsolidated materials; or at least 5 ft (1.5 m), but no more than 10 ft (3.0 m), for consolidated materials. In highly unstable formations, withdrawal intervals may be much less. After each increment, it should be ascertained that the primary filter pack has not been displaced during the withdrawal operation (using a weighed measuring device).

8.5 *Placement of First Secondary Filter*—A secondary filter pack may be installed above the primary filter pack to prevent the intrusion of the bentonite grout seal into the primary filter pack (see Figs. 1 and 2). To be effective, a measured and recorded volume of secondary filter material should be added to extend 1 to 2 ft (0.3 to 0.6 m) above the primary filter pack. As with the primary filter, a secondary filter must not extend into an overlying hydrologic unit (see 8.4.1). The well designer should evaluate the need for this filter pack by considering the gradation of the primary filter pack, the hydraulic heads between adjacent units, and the potential for grout intrusion into the primary filter pack. The secondary filter material is poured into the annular space through a decontaminated, flush threaded, 1-in. (25-mm) minimum internal diameter tremie pipe lowered to within 3 ft (1.0 m) of the placement interval. Water from a source of known and acceptable chemistry may be added to help deliver the filter pack to its intended location. The tremie pipe or a weighed line can be used to measure the top of the secondary filter pack as work progresses. The elevation (or depth below ground surface), volume, and gradation of the secondary filter pack should be recorded on the well completion diagram.

8.6 *Installation of the Bentonite Seal*—A bentonite pellet or a slurry seal is placed in the annulus between the borehole and the riser pipe on top of the secondary or primary filter pack (see Figs. 1 and 2). This seal retards the movement of cement-based grout backfill into the primary or secondary filter packs. To be effective, the bentonite seal should extend above the filter packs approximately 3 to 5 ft (1.0 to 1.5 m), depending on local conditions. The bentonite slurry seal should be installed using a positive displacement pump and a side-discharge tremie pipe lowered to the top of the filter pack. The tremie pipe should be raised slowly as the bentonite slurry fills the annular space. Bentonite pellets or chips may be poured from the surface and allowed to free-fall into the borehole. As a bentonite pellet or chip seal is poured into the borehole, a tamper may be necessary to tamp pellets or chips into place or to break bridges formed as the pellets or chips stick to the riser or the walls of the water-filled portion of the borehole. If the bentonite seal is installed above the water level in the borehole, granular bentonite should be used as the seal material – *bentonite pellets or chips should not be used in the unsaturated zone*. Granular bentonite should be poured into the borehole and installed in lifts of 2 in., then hydrated with water from a source of known chemistry. The tremie pipe or a weighed line can be used to measure the top of the bentonite seal as the work progresses. Sufficient time should be allowed for the bentonite pellet seal to hydrate or the slurry annular seal to expand prior to grouting the remaining annulus. The volume and elevation (or depth below ground surface) of the bentonite seal material should be measured and recorded on the well completion diagram.

8.7 *Final Secondary Filter Pack*—A 6-in. to 1-ft (0.15 to 0.3-m) secondary filter may be placed above the bentonite seal in the same manner described in 8.5 (see Figs. 1 and 2). This secondary filter pack will provide a layer over the bentonite seal to limit the downward movement of cement-based grout backfill into the bentonite seal. The volume, elevation (or depth below ground surface), and gradation of this final secondary filter pack should be documented on the well completion diagram.

8.8 *Grouting the Annular Space*:

8.8.1 *General*—Grouting procedures vary with the type of well design. The following procedures will apply to both single- and multi-cased monitoring wells. Paragraphs 8.8.2 and 8.8.3 detail those procedures unique to single- and multi-cased installations, respectively.

8.8.1.1 *Volume of Grout*—An ample volume of grout should be mixed on site to compensate for unexpected losses to the formation. The use of alternate grout materials, including grout containing gravel, may be necessary to control zones of high grout loss. The volume and location of grout used to backfill the remaining annular space is recorded on the well completion diagram.

8.8.1.2 *Grout Installation Procedures*—The grout should be pumped down hole through a side-discharge tremie pipe using a positive displacement pump (e.g., a diaphragm pump, moyno pump, or similar pump) to reduce the chance of leaving voids in the grout, and to displace any liquids and drill cuttings that may remain in the annulus. In very shallow wells, grouting may be accomplished by gravity feeding grout through a tremie pipe. With either method, grout should be introduced in one continuous operation until full-strength grout flows out of the borehole at the ground surface without evidence of drill cuttings, drilling fluid, or water.

8.8.1.3 *Grout Setting and Curing*—The riser should not be disturbed until the grout sets and cures for the amount of time necessary to prevent a break in the seal between the grout and riser. The amount of time required for the grout to set or cure will vary with the grout mix and ambient temperature and should be documented on the well completion diagram.

8.8.2 *Specific Procedures for Single-Cased Wells*—Grouting should begin at a level directly above the final secondary filter pack (see Fig. 1) if used, or above the bentonite pellet, chip or slurry seal. Grout should be pumped using a side-discharge tremie pipe to dissipate the fluid-pumping energy against the borehole wall and riser, reducing the potential for infiltration of grout into the primary filter pack. The tremie pipe should be kept full of grout from start to finish, with the discharge end of the pipe completely submerged as it is slowly and continuously lifted. Approximately 5 to 10 ft (1.5 to 3.0 m) of tremie pipe should remain submerged until grouting is complete. For deep installations or where the joints or couplings of the selected riser cannot withstand the collapse stress exerted by a full column of grout as it is installed, a staged grouting procedure may be used. If used, the drive/temporary casing or hollow-stem auger should be removed in increments immediately following each increment of grout installation and before the grout begins to set. If casing removal does not commence until grout pumping is completed, then, after the casing is removed, additional grout may be periodically pumped into the annular space to maintain a continuous column of grout up to the ground surface.

8.8.3 *Specific Procedures for Multi-Cased Wells*—If the outer casing of a multi-cased well cannot be driven to form a tight seal between the surrounding stratum (strata) and the casing, it should be installed in a pre-drilled borehole. After the borehole has penetrated not less than 2 ft. (0.6 m) of the first targeted confining stratum, the outer casing should be lowered to the bottom of the boring and the annular space pressure grouted. Pressure grouting requires the use of a grout shoe or packer installed at the end of the outer casing to prevent grout from moving up into the casing. The grout must be allowed to cure and form a seal between the casing and the borehole prior to advancing the hole to the next hydrologic unit. This procedure is repeated as necessary to advance the borehole to the desired depth. Upon reaching the final depth, the riser and screen should be set through the inner casing. After placement of the filter packs and bentonite seal, the remaining annular space is grouted as described in 8.8.2 (see Fig. 2).

NOTE 15—When using a packer, pressure may build up during grout injection and force grout up the sides of the packer and into the casing.

8.9 *Well Protection*—Well protection refers specifically to installations made at the ground surface to deter unauthorized entry to the monitoring well, to prevent damage to or destruction of the well, and to prevent surface water from entering the annulus. The methods described in Practice D 5787 should be used for well protection.

8.9.1 *Protective Casing*—Protective casing should be used for all monitoring well installations. In areas that experience frost heaving, the protective casing should extend from below the depth of frost penetration (3 to 5 ft [1.0 to 1.5 m] below grade, depending on local conditions), to slightly above the top of the well casing. The protective casing should be initially placed before final set of the grout. The protective casing should be sealed and immobilized in concrete placed around the outside of the protective casing above the set grout. The protective casing should be stabilized in a position concentric with the riser (see Figs. 3 and 1). Sufficient clearance, usually 6 in. (0.15 m) should be maintained between the lid of the protective casing and the top of the riser to accommodate sampling equipment. A ¼-in. (6.3-mm) ddiameter weep hole should be drilled in the protective casing approximately 6 in. (15 cm) above ground surface to permit water to drain out of the annular space between the protective casing and the riser. In cold climates, this hole will also prevent water freezing between the protective casing and the well casing. Dry bentonite pellets, granules, or chips should then be placed in the

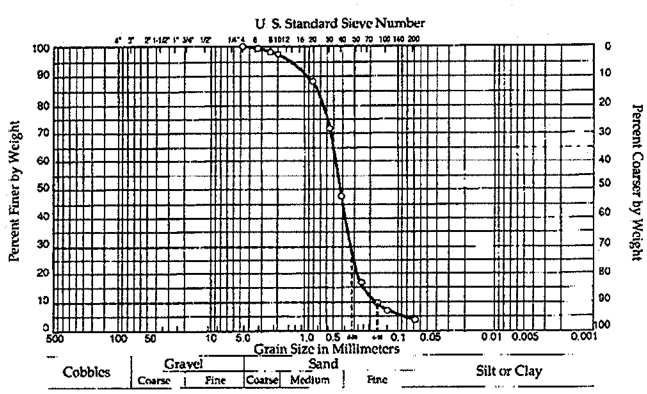



**FIG. 3 Example Grading Curve for Design of Monitoring Well Screens**

annular space below ground level within the protective casing. Coarse sand or pea gravel or both should be placed in the annular space above the dry bentonite pellets and to just above the weep hole to prevent entry of insects. All materials chosen should be documented on the well completion diagram. The monitoring well identification number should be clearly visible on the inside and outside of the protective casing.

8.9.2 *Completion of Surface Installation*—The well protection installation may be completed in one of three ways:

8.9.2.1 In areas subject to frost heave, place a soil or bentonite/sand layer adjacent to the protective casing sloped to direct water drainage away from the well.

8.9.2.2 In regions not subject to frost heave, a concrete pad, sloped slightly to provide water drainage away from the well, should be placed around the installation.

8.9.2.3 Where monitoring well protection must be installed flush with the ground, an internal cap should be fitted on top of the riser within the manhole or vault. This cap should be leak-proof so that if the vault or manhole should fill with water, the water will not enter the well casing. Ideally, the manhole cover cap should also be leak-proof.

8.9.3 *Additional Protection*—In areas where there is a high probability of damaging the well (high traffic, heavy equipment, poor visibility), it may be necessary to enhance the normal protection of the monitoring well through the use of posts, markers, signs, or other means, as described in Practice D 5787. The level of protection should meet the damage threat posed by the location of the well.

## 9. Well Development

9.1 *General*—Well development serves to remove fine-grained material from the well screen and filter pack that may otherwise interfere with water quality analyses, to restore the formation properties disturbed during the drilling process, and to improve the hydraulic characteristics of the filter pack and hydraulic communication between the well and the hydrologic unit adjacent to the well screen. Methods of well development vary with the physical characteristics of hydrologic units in which the monitoring well is screened and with the drilling method used.

9.2 *Development Methods and Procedures*—The methods and procedures for well development described in Guide D 5521 should be followed to ensure a proper well completion.

9.3 *Timing and Duration of Well Development*—Well development should begin either after the riser, well screen and filter pack are installed and before the bentonite seal and grout are installed (the preferred time), or after the monitoring well is completely installed and the grout has cured or set. In the former case, the installer may add filter pack material to the borehole before the bentonite seal is installed to compensate for settlement that typically occurs during the development process. This allows the installer to maintain the desired separation between the top of the screen and the bentonite seal. In the latter case, the possibility exists that settlement of the filter pack may result in the bentonite seal settling into the top of the screen. Development should be continued until representative water, free of the drilling fluids, cuttings, or other materials introduced or produced during well construction, is obtained. Representative water is assumed to have been obtained when turbidity readings stabilize and the water is visually clear of suspended solids. The minimum duration of well development will vary with the method used to develop the well. The timing and duration of well development and the turbidity measurements should be recorded on the well completion diagram.

9.4 *Well Recovery Test*—A well recovery test should be performed immediately after and in conjunction with well development. The well recovery test provides an indication of well performance and provides data for estimating the hydraulic conductivity of the screened hydrologic unit. Readings should be taken at intervals suggested in Table 2 until the well has recovered to 90 % of its static water level.

NOTE 16—If a monitoring well does not recover sufficiently for sampling within a 24-hr period and the well has been properly developed, the installation should not generally be used as a monitoring well for detecting or assessing low level organic constituents or trace metals. The installation may, however, be used for long-term water-level monitoring if measurements of short-frequency water-level changes are not required.

## 10. Installation Survey

10.1 *General*—The vertical and horizontal position of each monitoring well in the monitoring system should be surveyed and subsequently mapped by a licensed surveyor. The well location map should include the location of all monitoring wells in the system and their respective identification numbers, elevations of the top of riser position to be used as the reference point for water-level measurements, and the elevations of the ground surface protective installations. The locations and elevations of all permanent benchmark(s) and pertinent boundary marker(s) located on-site or used in the survey should also be noted on the map.

10.2 *Water-Level Measurement Reference*—The water-level measurement reference point should be permanently marked, for example, by cutting a V-notch into the top edge of the riser pipe. This reference point should be surveyed in reference to the nearest NAVD reference point.

10.3 *Location Coordinates*—The horizontal location of all monitoring wells (active or decommissioned) should be surveyed by reference to a standardized survey grid or by metes and bounds.

10.4 *Borehole Deviation Survey*—A borehole deviation survey, to determine the direction and distance of the bottom of the well relative to the top of the well and points in between, should be completed in wells deeper than 100 feet and in wells installed in dipping formations.

## 11. Monitoring Well Network Report

11.1 TTo demonstrate that the goals set forth in the Scope have been met, a monitoring well network report should be prepared. This report should:

**TABLE 2 Suggested Recording Intervals for Well Recovery Tests**

| Time Since Starting Test | Time Interval |
|---|---|
| 0 to 15 min | 1 min |
| 15 to 50 min | 5 min |
| 50 to 100 min | 10 min |
| 100 to 300 min (5 h) | 30 min |
| 300 to 1440 min (24 h) | 60 min |

11.1.1 Locate the area investigated in terms pertinent to the project. This should include sketch maps or aerial photos on which the exploratory borings, piezometers, sample areas, and monitoring wells are located, as well as topographic items relevant to the determination of the various soil and rock types, such as contours, streambeds, etc. Where feasible, include a geologic map and geologic cross sections of the area being investigated.

11.1.2 Include copies of all well boring test pits and exploratory borehole logs, initial and post-completion water levels, all laboratory test results, and all well completion diagrams.

11.1.3 Include the well installation survey.

11.1.4 Describe and relate the findings obtained in the initial reconnaissance and field investigation (Section 5) to the design and installation procedures selected (Sections 7-9) and the surveyed locations (Section 10).

11.1.5 This report should include a recommended decommissioning procedure that is consistent with those described in Guide D 5299 and/or with applicable regulatory requirements.

## 12. Keywords

12.1 aquifer; borehole drilling; geophysical exploration; ground water; monitoring well; site investigation